



BRIGHT PLAN CIVILS

**LAND AT THISTLEWORTH FARM,
GRINDERS LANE, DIAL POST RH13 8NR**

RE-PROFILING OF AGRICULTURAL LAND

Drainage Strategy Report

Prepared on Behalf of

Alfie Hyatt

2020/D1867B/DS1.2

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Re-Profiling of Agricultural Land

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1 INTRODUCTION

1.1 Background

- 1.1.1 Bright Plan Civils is instructed by Alfie Hyatt to prepare a Drainage Strategy Report to support a planning application for a Re-Profiling of Agricultural Land at the Land at Thistleworth Farm, Grinders Lane, Dial Post RH13 8NR.
- 1.1.2 The application for which this report refers is referred to as the application site within the report, and is situated within a wider area of land ownership of Thistleworth Farm. For the purposes of preparing a drainage strategy that uses best practice, the entire runoff catchment of which this application site is situated within has been assessed, in order to ensure that any proposed drainage system is not overwhelmed by greenfield runoff from the wider catchment.
- 1.1.3 This report has been undertaken in accordance with National Planning Policy Framework (NPPF) and The Planning Practice Guidance on the use of SuDS for achieving sustainable development.
- 1.1.4 The proposed application is for an area of raised land in order to improve the poor quality of agricultural land with excavated earth and clay from a neighbouring area of land under site ownership, as well as imported screened waste - as demonstrated within the preliminary site layout, contained within **Appendix A** of this report.
- 1.1.5 In preparing this report, Bright Plan Civils has referred to the following documents and information:
- Environment Agency Flood Maps for Planning
 - Long Term Flood Risk Information; Flood Risk Maps
 - Southern Water and Local Authority Drainage Records
 - British Geological Survey & Records
- 1.1.6 This document has been prepared to propose assess drainage constraints and propose a drainage strategy that is appropriate for the design life of the development, without causing offsite impacts from runoff in a design event.
- 1.1.7 This report has been prepared for the benefit of the named Client only.

1.2 Site Location and Description

- 1.2.1 The property is situated between the residential area and industrial area of Dial Post, situated just off the A24 between Horsham and Worthing, in West Sussex. The site is bounded by the A24 highway to the northwest, and agricultural land to the south and east.
- 1.2.2 A topographical survey of the site has been undertaken and provided by the client. It is included in **Appendix B** of this report.
- 1.2.3 The topographical survey shows that the site falls inwards towards the centre of the drainage catchment, and is enveloped by bunds to the north, east and west – as detailed in Drawing **100**.
- 1.2.4 The existing site is made up natural ground and imported soil, and is drained by a combination of

overland runoff and infiltration. There is no existing site drainage, however it will form part of the drainage assessment of a neighbouring application (screening site).

- 1.2.5 The nearest watercourse appears to be an ordinary watercourse northwest of the site, which runs northerly to the River Adur.
- 1.2.6 The nearest surface water feature is a pond at the head of the aforementioned ordinary watercourse, north of the site.
- 1.2.7 The existing application site has a total area of approximately 5,840m² (0.584 Ha), with no area existing or proposed to be hardstanding – as seen in Drawing **200**.

1.3 Ground Conditions

- 1.3.1 Two soakage holes were dug, one on the site and one on land also owned to the south. These were dug to approximately 2 metres deep. The excavated ground consisted of hardcore, gravel and topsoil to 1mbgl, with sandy clay to the depths of the boreholes.
- 1.3.2 Infiltration rates of 8.7×10^{-6} m/s, 9.1×10^{-6} m/s and 1.1×10^{-5} m/s were recorded at the two trial holes, with all three tests resulting in full emptying of water. This would indicate there is potential for the use of infiltration SuDS, however the infiltration may be in part to lateral drainage through the infill hardcore and other deposited soils, at the concern is that this would not be infiltrated into the underlying Clay through infiltration methods. The infiltration test results can be seen in **Appendix C**.
- 1.3.3 In addition to site-specific soakage testing, reference has been made to the British Geological Survey (BGS) website.
- 1.3.4 The BGS geology viewer states that the bedrock geology is likely to consist of 'Weald Clay Formation - Mudstone', as seen in **Figure 1**.



Figure 1. BGS website Bedrock geology

- 1.3.5 No Superficial Deposits are recorded at the site.

- 1.3.6 Historic borehole records from the Single Onshore Boreholes Index (SOBI) on the BGS website have also been reviewed in the absence of a site-specific geotechnical investigation, as depicted in **Figure 2**.

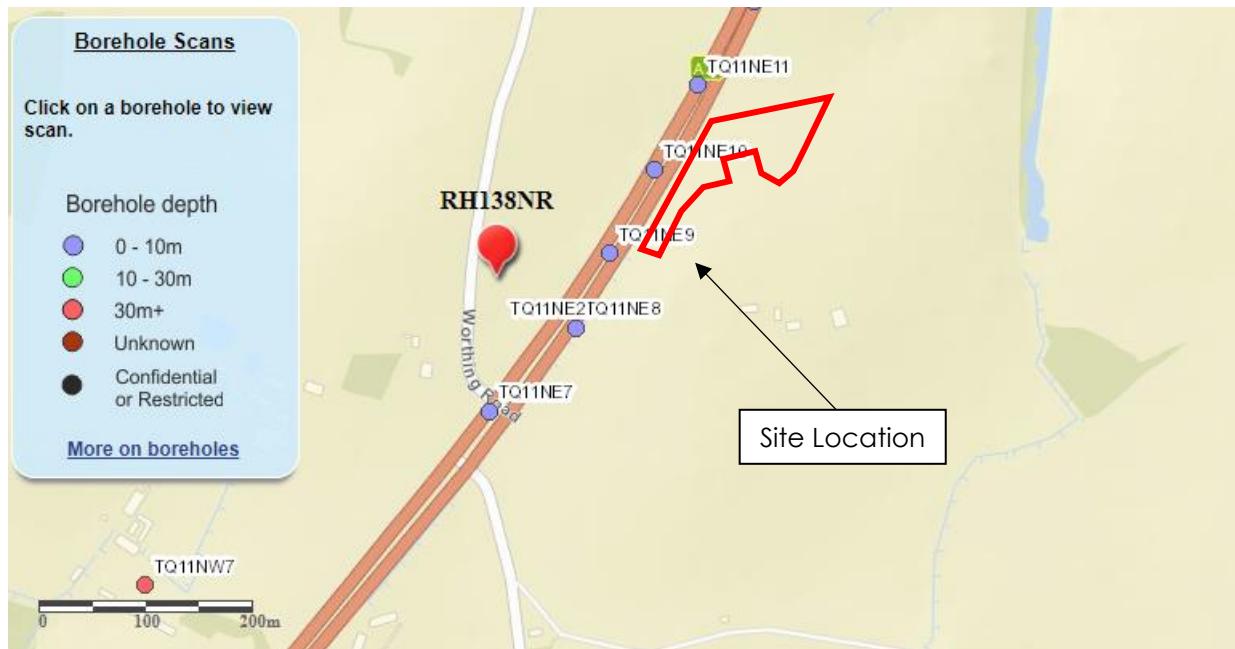


Figure 2. BGS website borehole locations

- 1.3.7 Two boreholes along the west boundary of the site were assessed in comparison to the site, as seen in **Figure 2**. These had similar geotechnical strata according to the BGS online mapping.
- 1.3.8 The logs stated that the geological composition encountered consisted of grey sandy silty clay for the depth of the boreholes.
- 1.3.9 A copy of the BGS records reviewed can be found within **Appendix D** of this report.

1.4 Groundwater

- 1.4.1 The excavated boreholes did not encounter groundwater, however there was seepage into one of the holes (within the screening site to the south). This was considered to be from an existing French Drain that intercepted the hole, and was partially the reason the holes were excavated deeper to extend beyond the depths of the French Drain and allow for soakage testing into the underlying Clay.
- 1.4.2 The recorded BGS boreholes did not encounter groundwater.
- 1.4.3 The Horsham District SFRA makes no mention of the settlement of Dial Post, and references to groundwater are limited to the southern extent of the study area.
- 1.4.4 Mapping managed by MAGIC (magic.defra.gov.uk) provides geographic information concerning the natural environment from across government. This mapping tool has been referred to in order to confirm whether the site is located within either any groundwater source protection zones or groundwater vulnerability zones.
- 1.4.5 The site is situated within a 'Unproductive' Aquifer for both Bedrock and Superficial Drift stratum, as seen in **Figure 3**. This refers to drift deposits and bedrock geology that are not considered to exhibit significant infiltration, and do not contribute significant groundwater to an aquifer or river supply.

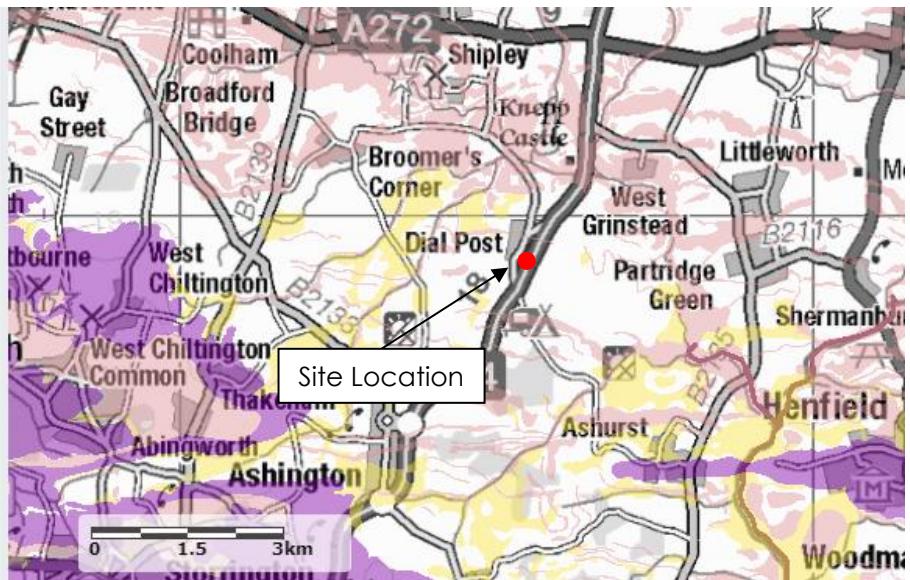
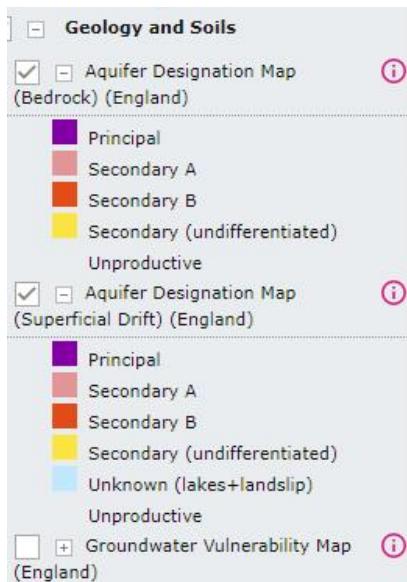


Figure 3. DEFRA Aquifer Designation Map

- 1.4.6 The Groundwater Vulnerability Map (**Figure 4**) confirms that the site falls within a 'Unproductive' groundwater vulnerability zone.

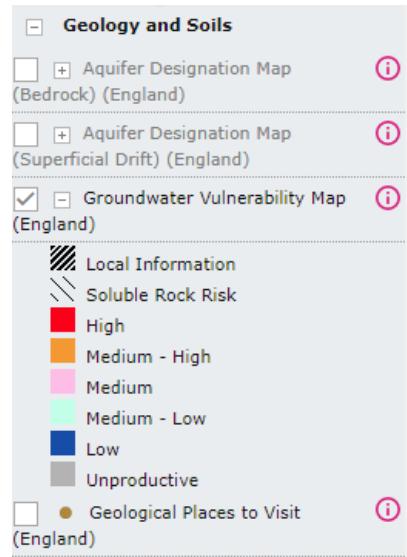


Figure 4. DEFRA Groundwater Vulnerability Map

- 1.4.7 The site is not indicated as within or in the vicinity of any Drinking Water Safeguard Zone or a Source Protection Zone.

1.5 Existing Drainage

- 1.5.1 The local Water Authority is Southern Water, who provide sewerage services within the area. Public sewer records have been obtained from Southern Water, as contained within this report in **Appendix E**.
- 1.5.2 Surface Water:
- The Southern Water public sewer records (**Appendix E**) show no public surface water sewers within the vicinity of the site.

- The existing site is made up natural ground and coarse hardcore, and is believed to be drained by a combination of overland runoff and infiltration. An existing French Drain was found running along the western boundary at the bottom of the bund within the screening site to the south, encountered during geotechnical investigations.
- The nearest watercourse appears to be an ordinary watercourse that runs adjacent to the site, before being culverted and re-appearing north of the site, which runs northerly to the River Adur.
- The nearest surface water feature is a pond at the re-issue of the aforementioned ordinary watercourse, north of the site.
- Greenfield runoff rate (Q_{bar}) for the drainage catchment has been calculated to be 10.88l/s, based on an area of 1.9Ha.

1.5.3 Foul Water:

- The Southern Water public sewer records (**Appendix E**) show that there are no public foul sewers in the vicinity of the site.
- At present, there is no confirmation of the foul water connection from the site, and investigation is required to establish connection arrangements should it be required for the proposed development.

1.5.4 Highway Drainage:

- The adjacent highway (private road) appears to be drained by overland runoff.

2 FLOOD RISK

2.1 Flood Maps and Modelling

- 2.1.1 The Environment Agency's on-line Flood Maps for Planning (rivers and sea) show that the site is located within Flood Zone 1, and not in the vicinity of any other flood zones.

Flood Zone	Definition
Zone 1 Low Probability	Land having a less than 1 in 1,000 annual probability of river or sea flooding. (Shown as 'clear' on the Flood Map – all land outside Zones 2 and 3)
Zone 2 Medium Probability	Land having between a 1 in 100 and 1 in 1,000 annual probability of river flooding; or land having between a 1 in 200 and 1 in 1,000 annual probability of sea flooding. (Land shown in light blue on the Flood Map)
Zone 3a High Probability	Land having a 1 in 100 or greater annual probability of river flooding; or Land having a 1 in 200 or greater annual probability of sea flooding. (Land shown in dark blue on the Flood Map)
Zone 3b The Functional Floodplain	This zone comprises land where water has to flow or be stored in times of flood. Local planning authorities should identify in their Strategic Flood Risk Assessments areas of functional floodplain and its boundaries accordingly, in agreement with the Environment Agency. (Not separately distinguished from Zone 3a on the Flood Map)

- 2.1.2 **Figure 5** also shows that the site is not at risk of flooding from rivers or sea.

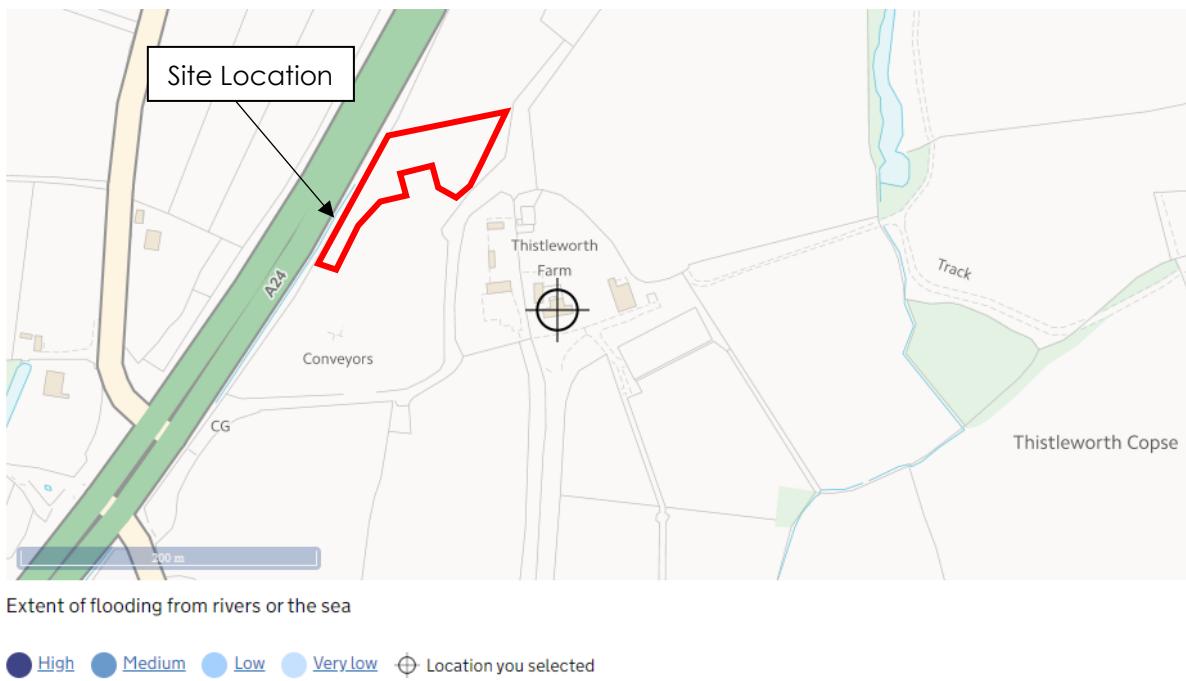


Figure 5. Long Term Flood Risk Map; Flood risk from rivers or the sea

- 2.1.3 **Figure 6** shows that the site at 'very low' to 'low' risk of surface water flooding, however the adjacent highway to the west is at 'high' risk of surface water flooding. The site is significantly elevated above the

highway with a large highway ditch and a boundary bund between the site and the highway, so it is not expected that the highway surface water flow path would affect the site. Depths along the access road to the site are shown to be between 300mm and 900mm in a low risk scenario however, which could affect access and egress.

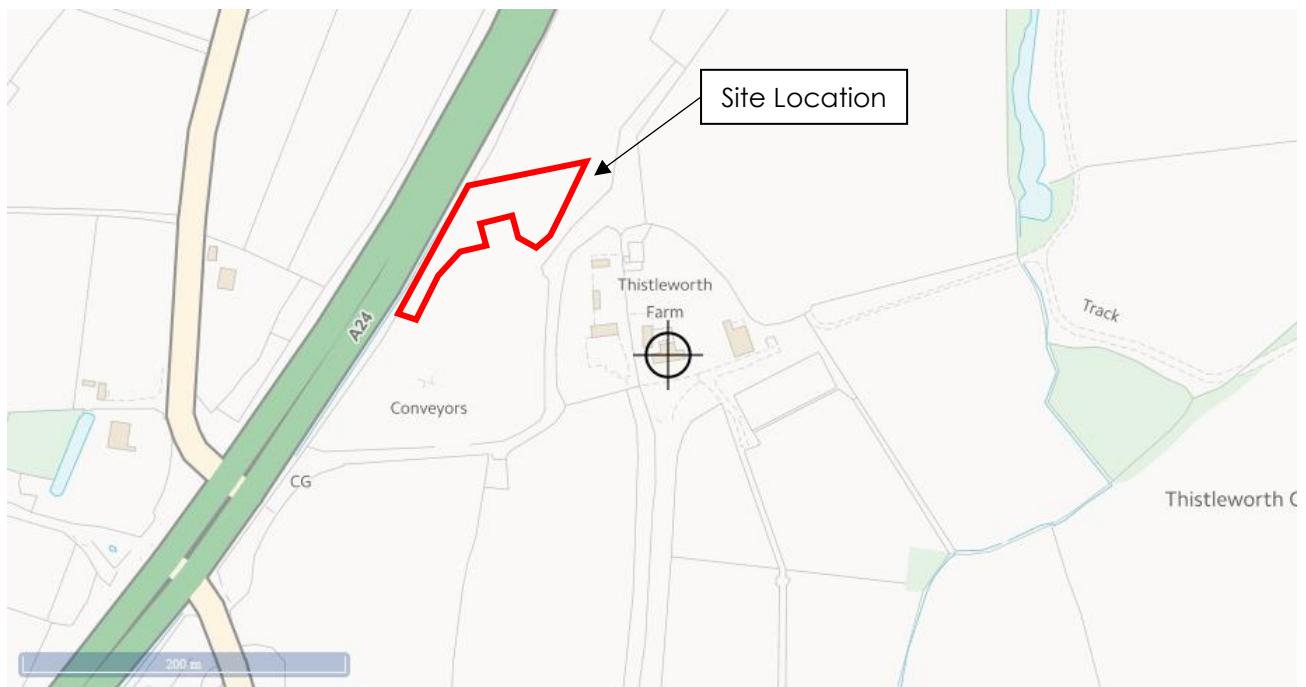


Extent of flooding from surface water

● High ● Medium ● Low ● Very low ○ Location you selected

Figure 6. Long Term Flood Risk Map; Flood risk from surface water

2.1.4 **Figure 7** shows that the site is not at risk of flooding from reservoirs.



Extent of flooding from reservoirs

● Maximum extent of flooding ○ Location you selected

Figure 7. Long Term Flood Risk Map; Flood risk from reservoirs

2.2 Summary of Flood Risk

2.2.1 The potential sources of flooding are:

Source of Flooding	Level of Risk
Rivers and Coastal	Very Low The site is within Flood Zone 1 as is the surrounding area. The site is not in the vicinity of any watercourses or tidal sources.
Surface Water	Low The long-term flood risk for surface water is classified as 'low' along the west of the site. Although this area of the site is significantly raised above the adjacent highway, the access road may be susceptible to surface water flooding of up to 900mm inhibiting access and egress.
Groundwater	Low BGS records found the site to be situated above unproductive strata, and nearby borehole logs did not find any presence of shallow groundwater. The Horsham SFRA did not indicate the site area as susceptible to groundwater flooding.
Sewers	Low There are no surface water sewers within the area, and no reports of sewer flooding found. The site is significant raised by several metres above the highway and adjacent highway drainage ditch at risk of being surcharged. In view of this information the risk of flooding from this source is deemed to be 'Low'.
Artificial Sources	None The site is not shown to be at risk of flooding due to artificial sources.

2.2.2 The site is not considered to be vulnerable to flood risk from any of the above assessed sources, however the proposed drainage system for the proposed development should be designed in order to provide capacity up to the design event and provide consideration of potential exceedance routes, so as to not increase the risk of surface water flooding on or off the site.

3 PROPOSED DRAINAGE STRATEGY

3.1 Surface Water

- 3.1.1 The SUDS manual and Building Regulations set out a hierarchy of drainage methods to ensure that developments maximise the use of sustainable drainage techniques. The hierarchy favours infiltration methods of disposal over other methods such as watercourse and sewers, as detailed below;
- i. Utilise infiltration techniques
 - ii. Attenuate rainwater in ponds or open water features for gradual release
 - iii. Attenuate rainwater by storing in tanks or sealed water features for gradual release
 - iv. Discharge rainwater direct to a watercourse
 - v. Discharge rainwater to a surface water sewer/drain
 - vi. Discharge rainwater to a combined sewer

SUDS Technique	Suitable	Comments
Living Roof	No	No significant building proposals.
Basins and Ponds (such as Wetlands, Balancing Ponds, Detention Basins, Retention Ponds)	Yes	Would provide attenuation as well as ecological benefits. No space available within screening site but surrounding land under same ownership.
Filter strips and swales	Yes	Would capture, filter and attenuate overland runoff.
Infiltration Devices - Soakaways - Infiltration trenches and basins	No	Underlying ground conditions are not indicated as permeable. Though site testing found some limited infiltration potential, there are concerns this is lateral soakage due to hardcore infill ground.
Permeable surfaces and filter drains (such as gravelled areas and porous block paving)	Yes	Permeable surfaces would also provide a source of treatment and shallow attenuation if tanked.
Tanked systems (such as oversized pipes or cellular tanks)	Yes	No initial constraints, would provide attenuation volume.

- 3.1.2 Despite the limited potential indicated by on-site soakage tests, it is not considered that infiltration measures are viable, given BGS borehole records in the vicinity which indicate underlying Clay from below the surface to bedrock level.
- 3.1.3 There are no hardstanding areas proposed within this application site, however the drainage strategy has been assessed in combination with the screening site to the south. This has been assessed and submitted under a separate drainage strategy, with pre-treatment of runoff from the industrial screening site prior to entering the shared pond.
- 3.1.4 Despite the land to the south not being part of this site planning application, this land is under the same ownership and also makes up part of the same drainage catchment. Appropriate capture and treatment of the runoff from the site has been considered in coordination with drainage of the catchment as a whole, given the area is landlocked by higher ground on all sides.
- 3.1.5 A balancing pond will therefore capture overland runoff from the catchment, as well as the proposed screening site of which there is 3,493m² of planned hardstanding areas, and discharge to the watercourse at a controlled rate of 8.0l/s, which is a betterment compared to the Greenfield rate of the catchment, as detailed in Drawing **PL300**.
- 3.1.6 Prior to connection to the watercourse, further information will be required to set out the details of the connection and approval of a Land Drainage Consent from WSCC will be required.
- 3.1.7 It is proposed that all captured runoff from the site is captured up to the 100-year event including 40% climate change without exceedance. Should the proposed drainage system be exceeded at the pond due to overland runoff from the catchment exceeding estimations, then the low-lying area around the pond would temporarily flood causing no significant flooding or access/egress issues to the screening site.
- 3.1.8 The strategy above will ensure that there is no increase in the rate of run-off leaving the site, therefore no increase in the risk of flooding from this source.

3.2 Treatment

- 3.2.1 In accordance with the CIRIA SuDS Manual C753 regarding methods for managing pollution risks, the risk posed by surface water runoff to the receiving environment depends on the pollution hazard at the site (the source), SuDS treatment techniques (the pathway), and the sensitivity of the environment (the receptor).
- 3.2.2 It is not considered that an assessment of treatment is needed for the proposed site, as this will remain Greenfield as previously, albeit raised due to imported ground.
- 3.2.3 As there is a risk of contamination from the screening site to the south, a separate planning application and drainage strategy has assessed the pre-treatment of runoff for the industrial screening site prior to its discharge to the shared pond.
- 3.2.4 This will form part of the on-site management regime for this site, separate to this application.

4 MAINTENANCE

4.1 Proposed Maintenance Regime

- 4.1.1 Maintenance is required to ensure the long-term operational performance of the proposed surface water drainage system.
- 4.1.2 The drainage system has been designed to minimise maintenance requirements; however a number of key tasks will need to be undertaken so that the system remains in optimal condition. These operations are summarised in the table below, along with the required frequency of works.

Drainage System feature	Proposed maintenance / remedial works	Required frequency of works
Pond & Filter Drain (surface)	Inspection, vegetation clearance and additional clearing/cleansing of potential surface blockages	At least once a year
	Inspection and clearance of blockages	After major storm events
Inlet, Outfall & Existing Watercourse	Inspection, vegetation clearance and additional clearing/cleansing of potential outfall blockages	At least once a year
	Desilting	Year 1, Year 3, then every 5 years
Pipework	Jetting to clear blockages	As required
Hydrobrake	As specified by manufacturer	As specified by manufacturer

- 4.1.3 The responsibility of maintenance regime will be determined by the Developer, by agreed appointment.

Pond

- 4.1.4 The pond will require additional maintenance measures to ensure they operate as designed. Failure in carrying out this maintenance, could increase the risk of flooding. The additional measures are as follows:
- Inspection, vegetation clearance and additional clearing/cleansing of potential surface blockages will be required on an annual basis.
 - Inspection and clearance of blockages after major storm events.

Inlet, Outfall & Existing Watercourse

- 4.1.5 A proposed inlet and outfall will be required for the discharge from the pond into the Flow Control Chamber and out to the boundary ditch. It is recommended that maintenance of the inlet and outfall features and the existing ditch is carried out to ensure conveyance off the site and prevent the risk of blockages and flooding, with measures as follows:

- Inspection, vegetation clearance and additional clearing/cleansing of potential outfall blockages will be required on an annual basis.
- Desilting is recommended at least as follows: On completion of drainage works, Year 1, Year 3, then every 5 years.

HydroBrake (Flow Control Chamber)

- 4.1.6 The HydroBrake flow control system is self-activating, relying on upstream hydraulic head to generate an air-filled vortex within the centre of the casing. Once the vortex is initiated water drains down through a small opening in the back of the device at the designed restricted flow rate.
- 4.1.7 The flow control device has two measures encase of emergency (i.e. blockage). The first is a door situated in the front of the unit itself, this can be operated from the surface by a release cable situated just under the manhole cover which closes under its own weight and does not require any mechanism to operate. The second is a high-level overflow pipe situated with the flow control manhole. Both measures allow the system to drain down freely, until the blockage can be cleared.
- 4.1.8 The HydroBrake flow control chamber will require additional maintenance measures to ensure it operates as designed. The additional measures are as follows:
- The sump within the flow control chamber should be monitored for build-up of silts and should be emptied, as a minimum, on the same regime as specified for catchpits previously within this document
 - The drain down door located on the centre of the unit will require inspection and opening annually, to ensure it is operating as intended

Remedial/Repair Actions

- 4.1.9 Significant storm events may cause considerable damage to SuDS and their associated components. As such, it may be necessary to inspect and carry out essential recovery works to return the features to full working order.

Accidental Spillages

- 4.1.10 It is not envisaged that any materials are to be stored onsite once the development has been completed, which could cause major spills and potential pollution issues within the drainage system. If this situation alters in the future consultation with a specialist will be required in order to confirm if any upgrades to the existing system are necessary.
- 4.1.11 Minor spillages of fuels and oils will be dealt with by the channel drains and bypass separators, by collecting and bio-degrading the hydrocarbons.

Future Alterations to the Development

- 4.1.12 Any future alterations to the drainage system components should be confirmed by a specialist. Where possible any future services are to avoid being located through areas of drainage system components. If new services are required to run through areas of drainage system components, services should be installed below the depth of drainage system components with the permeable system reinstalled above. If new uses of the site require an assessment of runoff treatment, this should be made and include provision of new drainage components if necessary.

5 SUMMARY

- 5.1.1 This site-specific flood risk assessment is based on Flood Maps, the Local Authority's Strategic Flood Risk Assessment, Site Investigation, BGS Records and Public Sewer Records.
- 5.1.2 The existing site consists of agricultural land. The site that the site falls inwards towards the centre of the drainage catchment, and is enveloped by bunds to the north, east and west. The site is part of surrounding land under the same ownership, and part of a runoff catchment within the land ownership land-locked from a runoff perspective
- 5.1.3 The area of the proposed screening site for which this report serves is 0.584Ha, and will have an impermeable area of 0.349Ha as a result of the development. The runoff catchment of 1.9Ha has been assessed for the purpose of preparation of the proposed surface water drainage system.
- 5.1.4 The proposed development is for an area of raised land in order to improve the poor quality of agricultural land with excavated earth and clay from a neighbouring area of land under site ownership, as well as imported screened waste.
- 5.1.5 The development lies within Flood Zone 1, with low or very low risk of surface water flooding. The existing run-off from the site is assumed to drain via a combination of infiltration (possibly laterally through infill soils and hardcore) and overland flow in the absence of confirmed existing drainage infrastructure.
- 5.1.6 Post-development surface water run-off will be managed through sustainable drainage measures, with runoff attenuated via a pond, without causing surface water flooding on site. Runoff to the watercourse will be limited via flow control devices.
- 5.1.7 The completion of the development will not increase flood risk on or off the site.
- 5.1.8 In conclusion, this development is suitable with regards to flood risk and surface water drainage.

DRAWINGS

- 100** Existing Topography & Overland Flow Routes
- 200** Impermeable Areas Comparison
- 300** Conceptual Drainage Strategy

NOTES

- This drawing is to be read in conjunction with all other RGP drawings, and with all relevant Architect's and Engineer's drawings and specification. Any discrepancies found are to be reported immediately to the Engineer.
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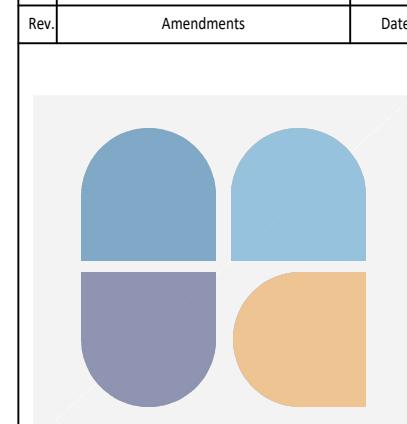
**-LEVELS KEY-**

- Land Ownership Boundary (36,750m²)
- Approximate Pond Catchment (18,700m²)
- Screening Site Boundary (8,540m²)
- Application Site Boundary (5,840m²)
- + 101.121 Existing Spot Level
- Existing Contour (Primary)
- Existing Contour (Secondary)
- Existing Gradient Arrow/Fall Direction
- HP Existing High Point
- LP Existing Low Point

Topographical information shown is based on survey undertaken by M.J. Zara Associates in May 2020. All levels relate to Ordnance Survey Datum via GPS. Contours are only as accurate as the initial land survey information.

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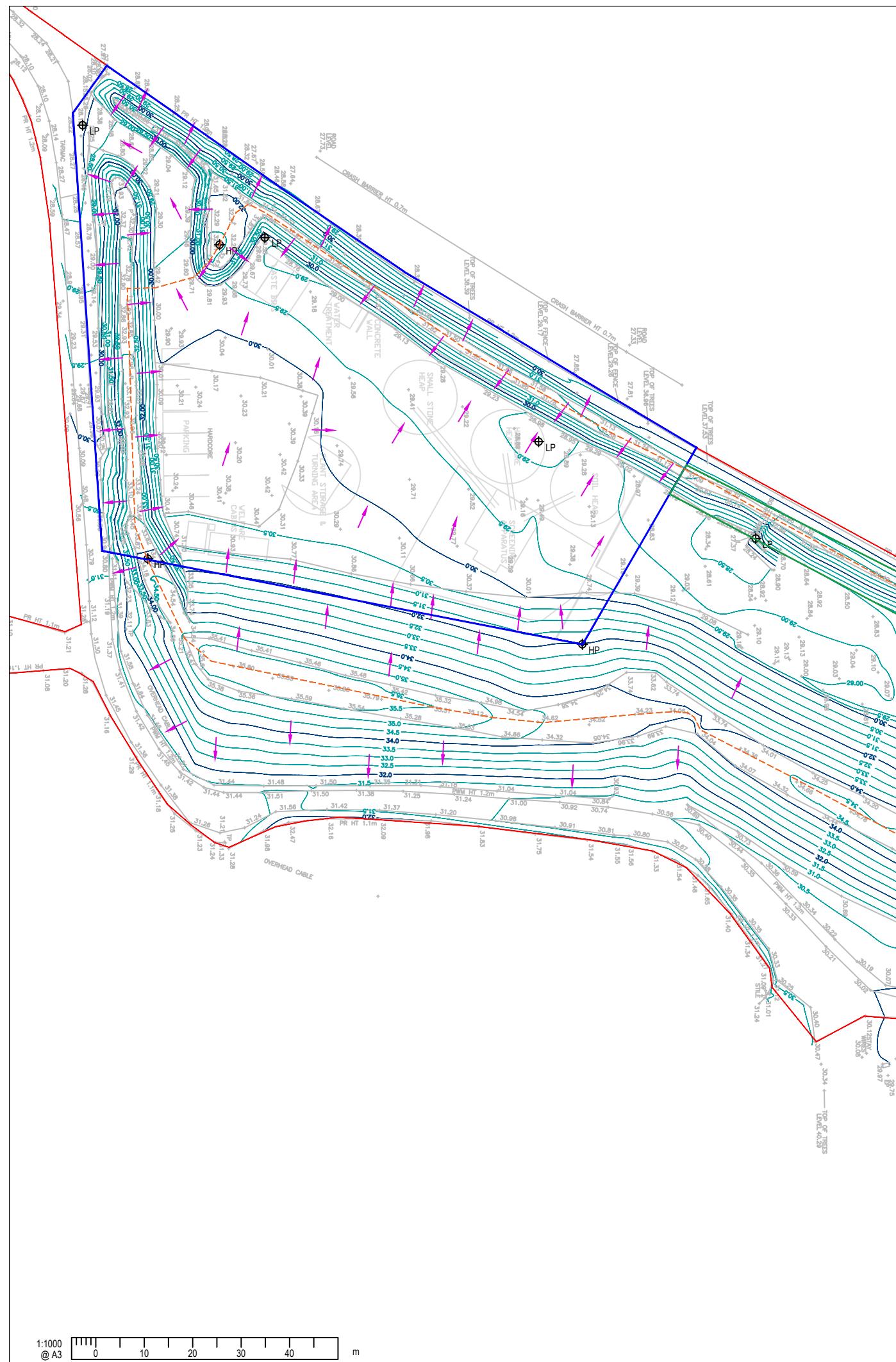
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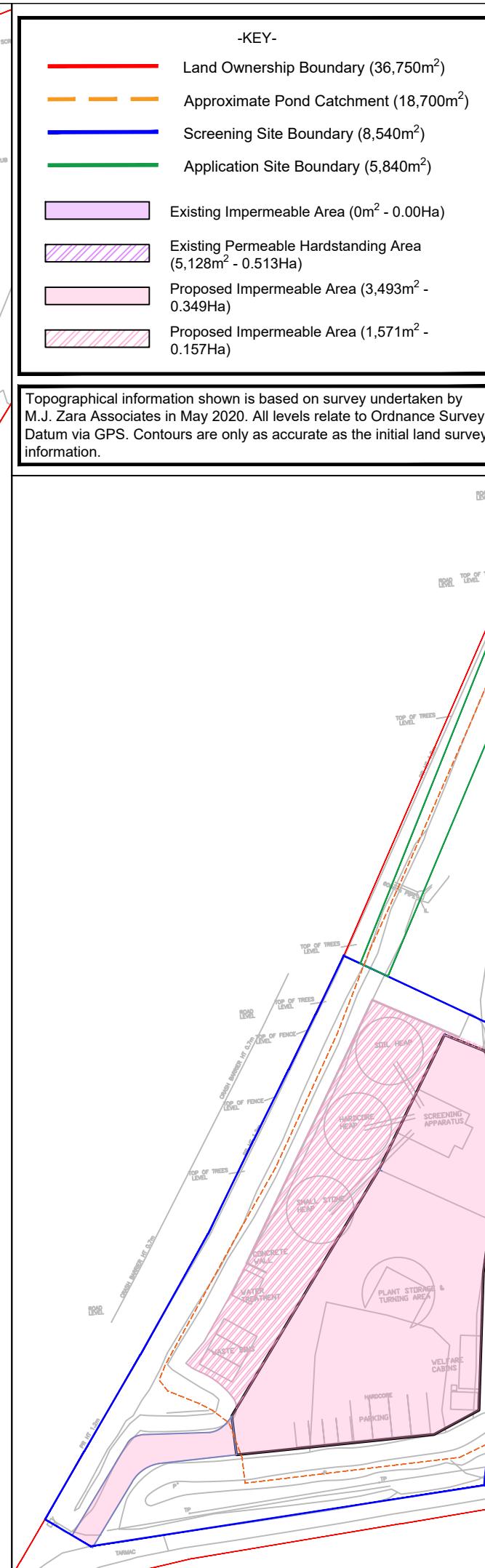
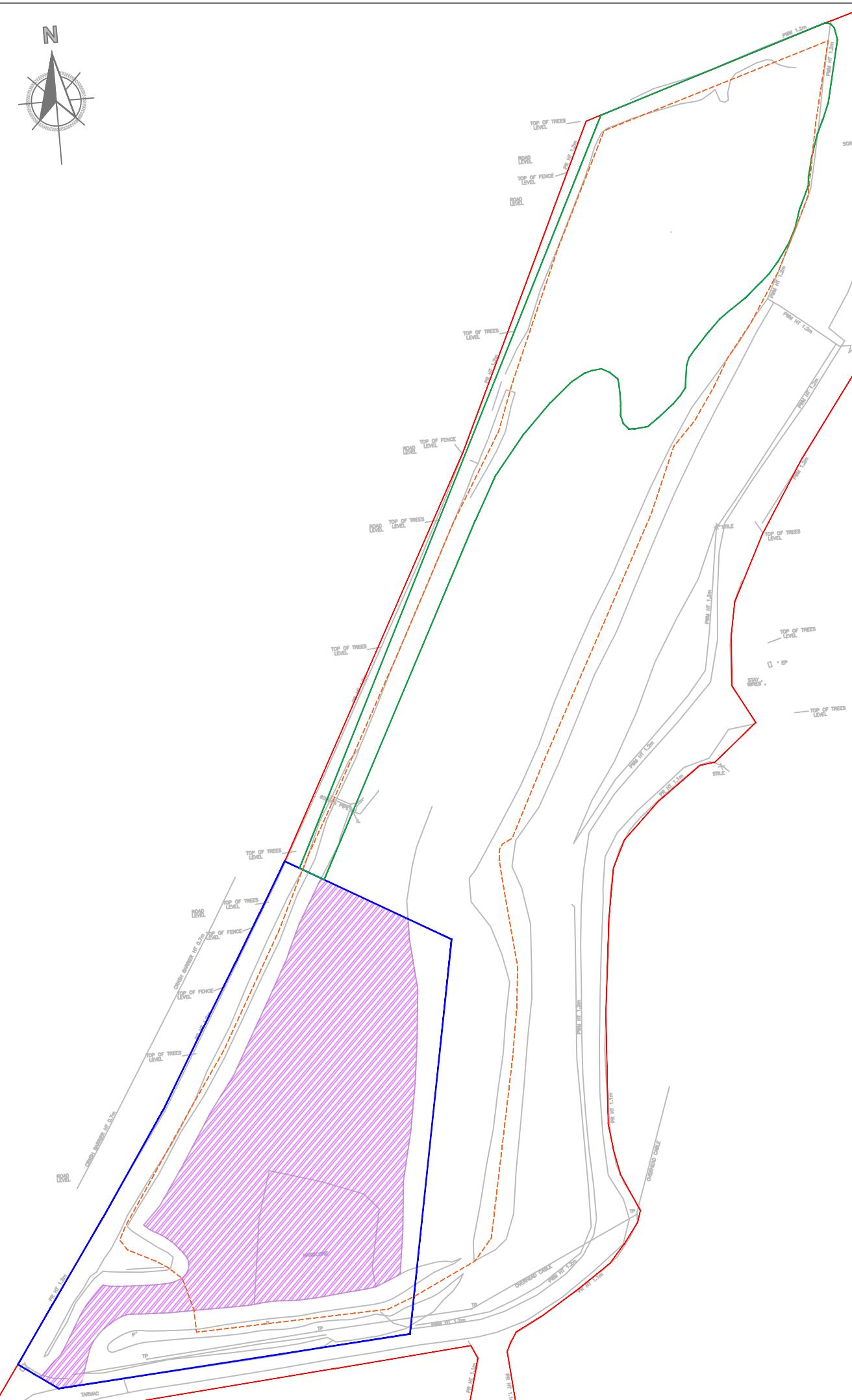
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Existing Topography & Overland Flow Routes

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Thistleworth Farm, Grinders Lane
Dial Post RH13 8NR

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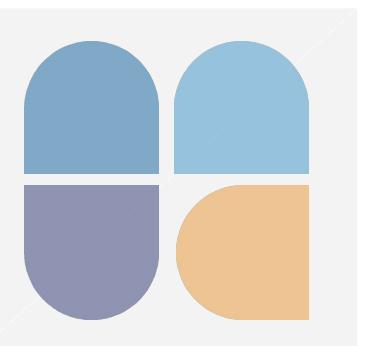
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- RGP accepts no responsibility for inaccuracies in data provided by third parties such as topographic surveys or Ordnance Survey mapping.
- Do not scale, work to figured dimensions only. All dimensions are in millimetres unless noted otherwise and all levels are in metres from the topographic survey datum.
- Any information given regarding existing underground services is given in good faith after consultation with the relevant authority, however accuracy is not certain.

PLANNING

NOT FOR CONSTRUCTION

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A	Revised Drawing	12/06/2020
Rev.	Amendments	Date



BRIGHT PLAN CIVILS
Transport Planning and Infrastructure Design Consultants
2 West Barn, Norton Lane, Chichester, West Sussex PO20 3AF
Tel: 01243 210418 Fax: 01243 861682
www.brightplancivils.co.uk

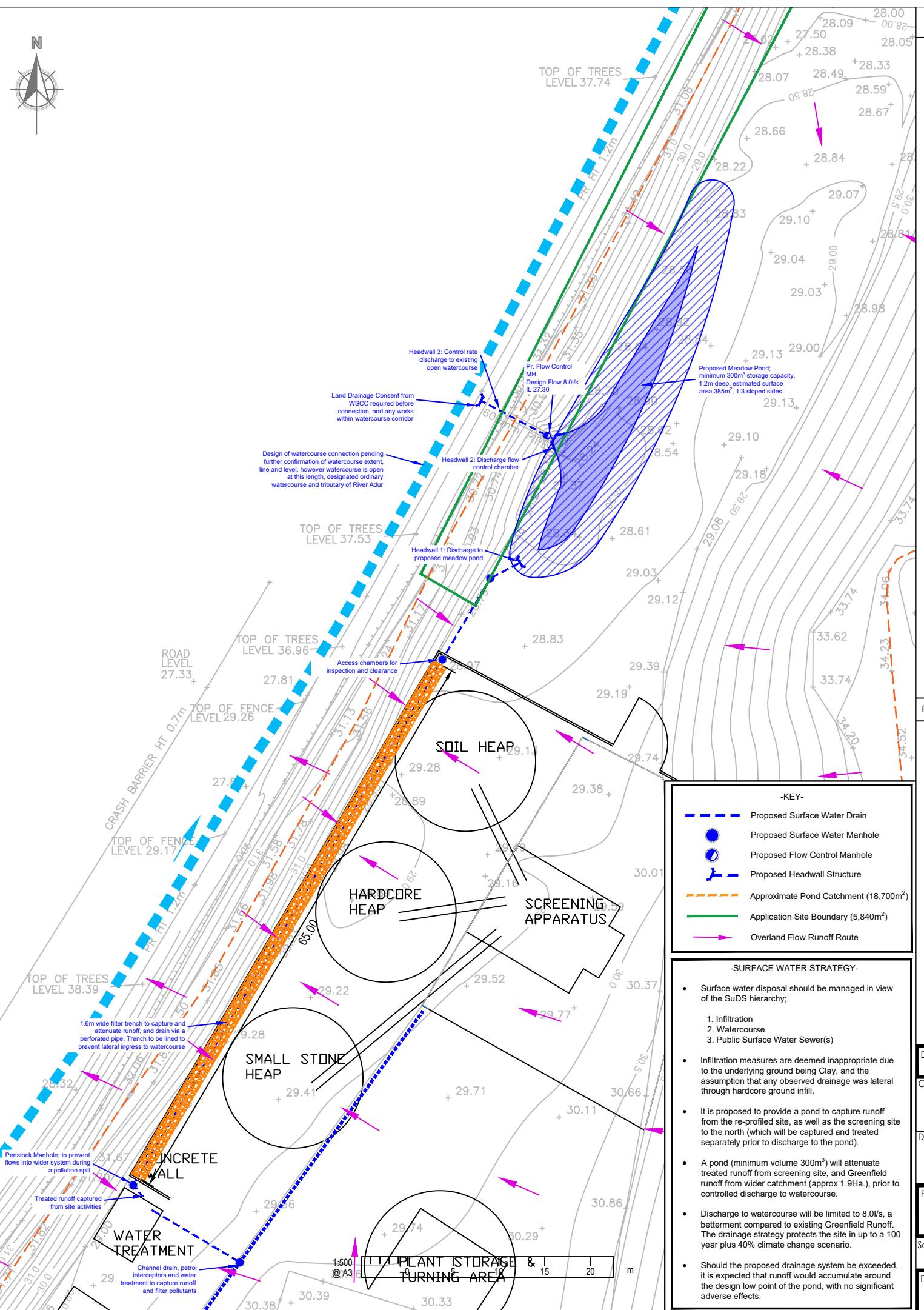
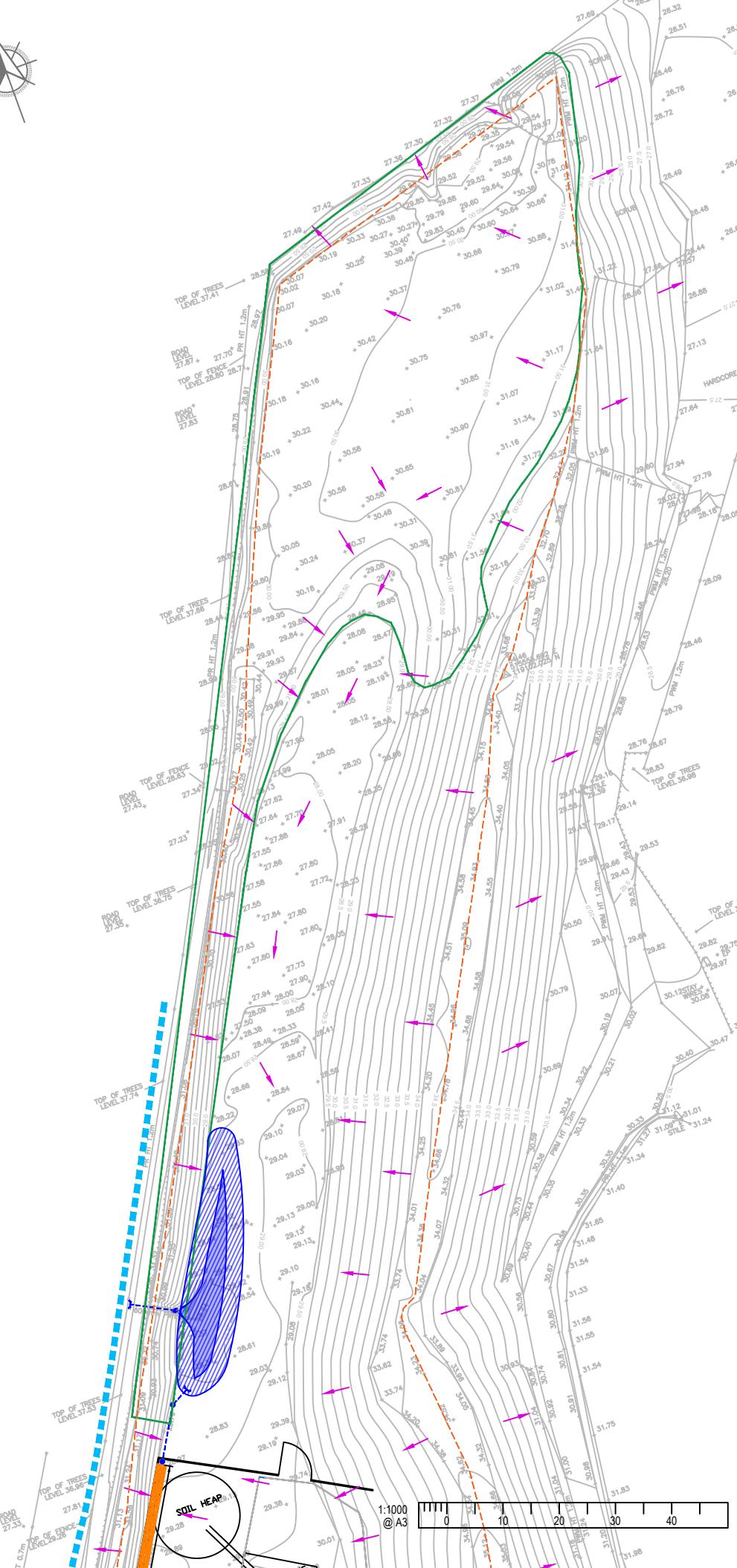
Drawing Status **PLANNING**
Client Alfie Hyatt

Drawing Title Conceptual Drainage Strategy

Project Thistleworth Farm, Grinders Lane
Dial Post, RH13 8NR

Scale VARIES Date June '20 Drawn By DJL Checked By MJA

Drawing No. D1867B-300 Rev. A



-KEY-	
Proposed Surface Water Drain	
Proposed Surface Water Manhole	
Proposed Flow Control Manhole	
Proposed Headwall Structure	
Approximate Pond Catchment (18,700m²)	
Application Site Boundary (5,840m²)	
Overland Flow Runoff Route	

- SURFACE WATER STRATEGY-**
- Surface water disposal should be managed in view of the SuDS hierarchy:
 - Infiltration
 - Watercourse
 - Public Surface Water Sewer(s)
 - Infiltration measures are deemed inappropriate due to the underlying ground being Clay, and the assumption that any observed drainage was lateral through hardcore ground infill.
 - It is proposed to provide a pond to capture runoff from the re-profiled site, as well as the screening site to the north (which will be captured and treated separately prior to discharge to the pond).
 - A pond (minimum volume 300m³) will attenuate treated runoff from screening site, and Greenfield runoff from wider catchment (approx 1.9Ha.), prior to controlled discharge to watercourse.
 - Discharge to watercourse will be limited to 8.0l/s, a betterment compared to existing Greenfield Runoff. The drainage strategy protects the site in up to a 100 year plus 40% climate change scenario.
 - Should the proposed drainage system be exceeded, it is expected that runoff would accumulate around the design low point of the pond, with no significant adverse effects.

APPENDICES



Appendix A Preliminary Site Layout

Notes

All dimensions must be checked on site and not scaled from this drawing.

If in doubt, please ask.

This drawing to be read in conjunction with all engineers and consultants drawings and specifications etc



LOCATION PLAN
1:2500

0 50 100 150
METRES
SCALE BAR 1:2500 @ A3

Project:
**THISTLEWORTH FARM
GRINDERS LANE
DIAL POST
WEST SUSSEX RH13 8NR-
PROPOSED
LAND-RAISING**

Drawing Title:
LOCATION PLAN
@ 1:2500

Client:
A HYATT CONTRACTORS LTD

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DOUGLAS J. P. EDWARDS
Chartered Building Surveyors
employing
Chartered Architects & Surveyors
Tel: 01403 740034
Email: info@douglasjpedwards.co.uk


Scale:
1:2500 @ A3 size
Date:
September 2020
Drawing No:
20-08-01

Project:
**THISTLEWORTH FARM
GRINDERS LANE
DIAL POST
WEST SUSSEX RH13 8NR-
PROPOSED
LAND-RAISING**

Drawing Title:
SITE PLAN @ 1:1000

Client:
A HYATT CONTRACTORS LTD

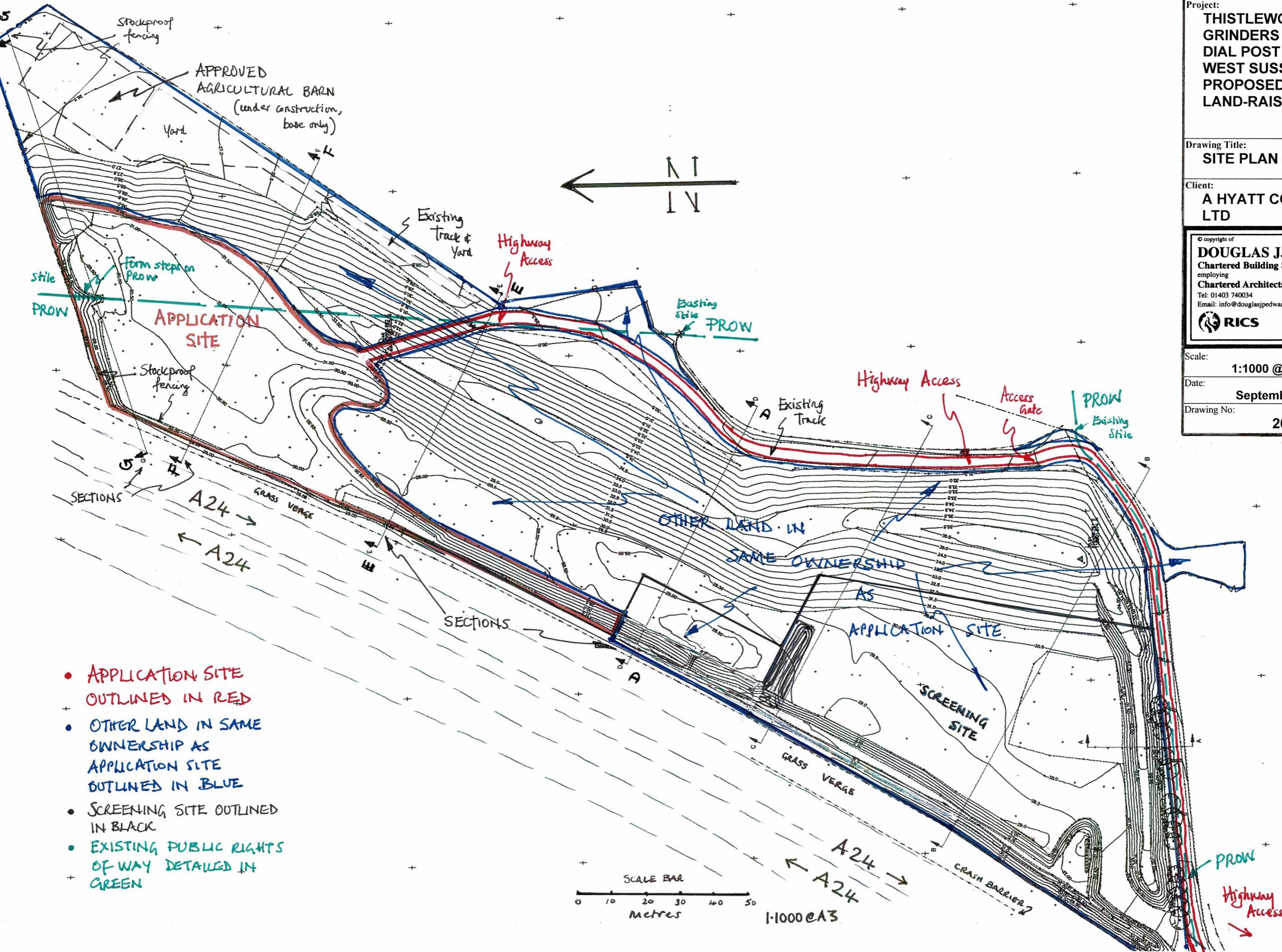
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Chartered Architects & Surveyors
Tel: 01403 740034
Email: info@douglasjpedwards.co.uk



Scale:
1:1000 @ A3 size

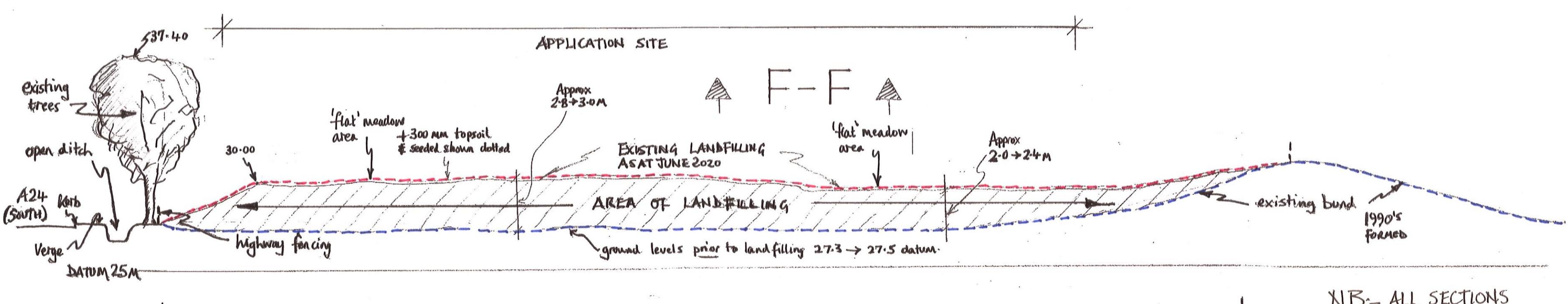
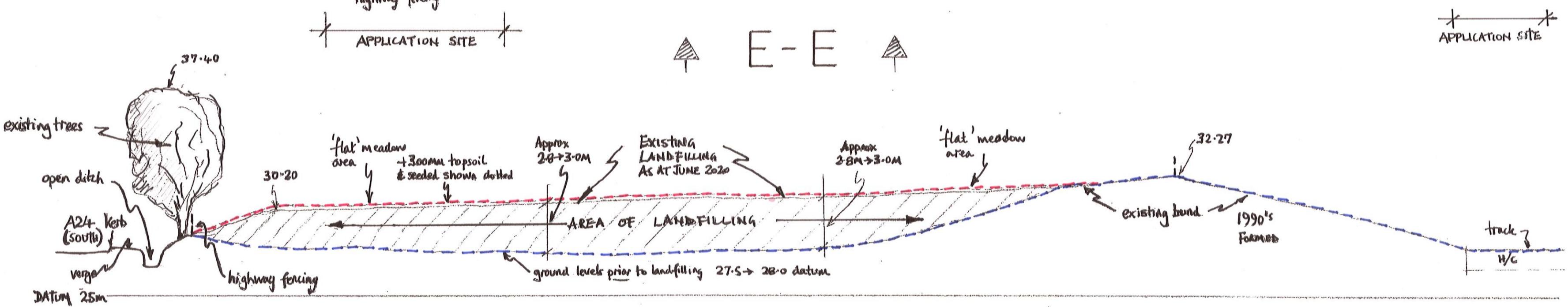
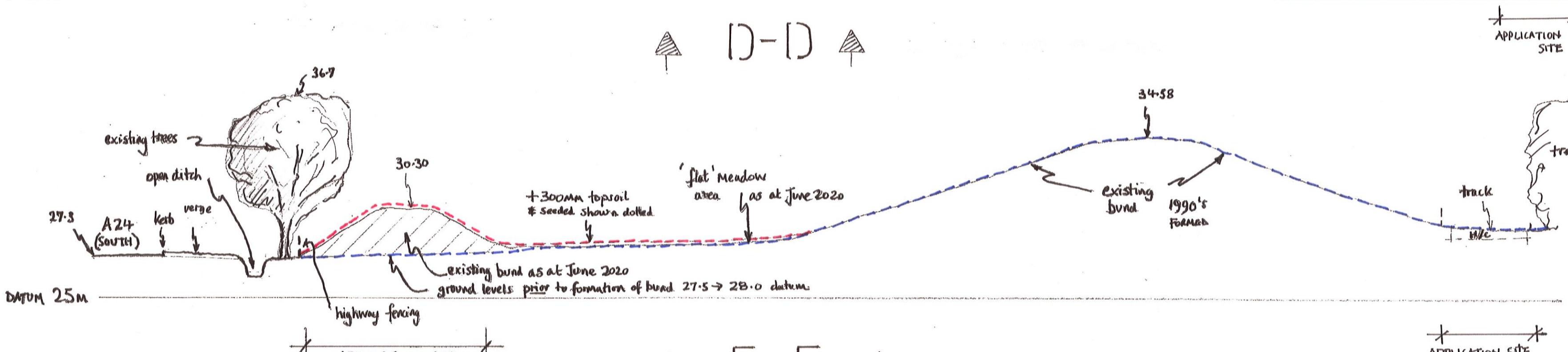
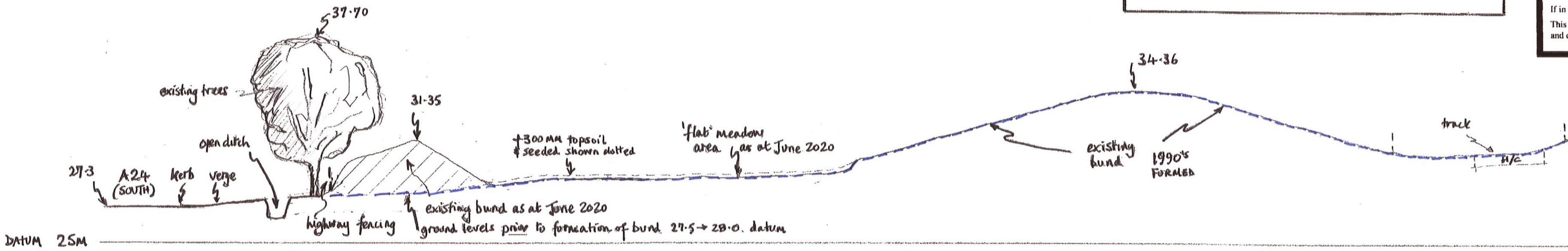
Date:
September 2020

Drawing No:
20-08-02



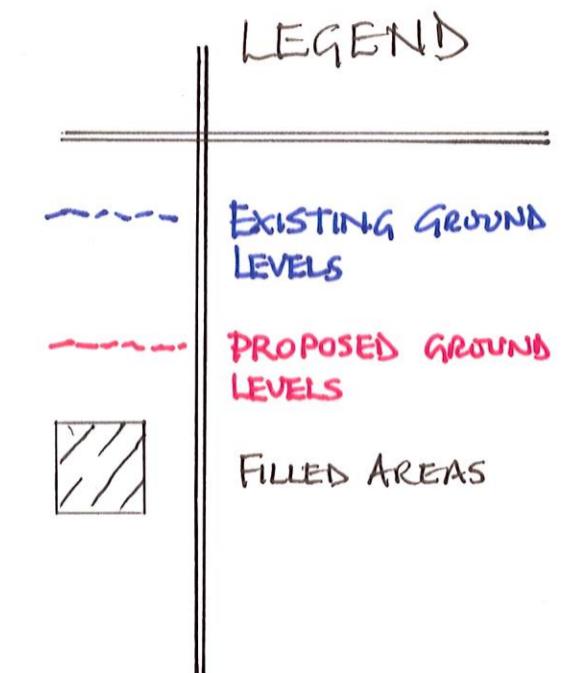
Notes

All dimensions must be checked on site and not scaled from this drawing.
If in doubt, please ask.
This drawing to be read in conjunction with all engineers and consultants drawings and specifications etc.



G-G [PART]

NB:- ALL SECTIONS
ARE LOOKING NORTHWARDS



Project:
**THISTLEWORTH FARM
GRINDERS LANE
DIAL POST
WEST SUSSEX RH13 8NR-
PROPOSED
LAND-RAISING**

Drawing Title:
SECTIONS D, E, F & G (part)

Client:
A HYATT CONTRACTORS LTD

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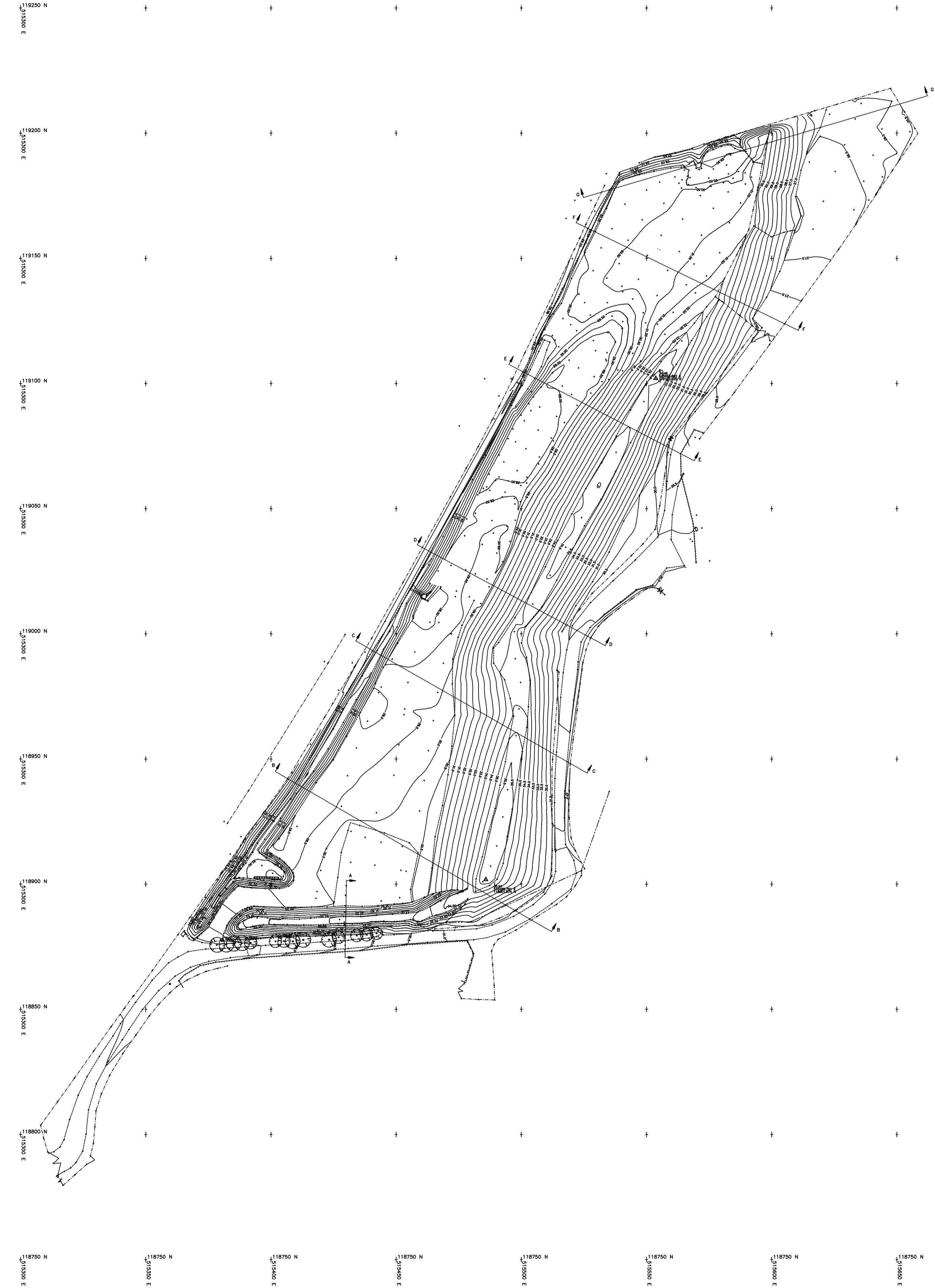
Scale:
1:200 @ A2 size

Date:
September 2020

Drawing No:
20-08-03



Appendix B Topographic Survey



LAYER INFORMATION

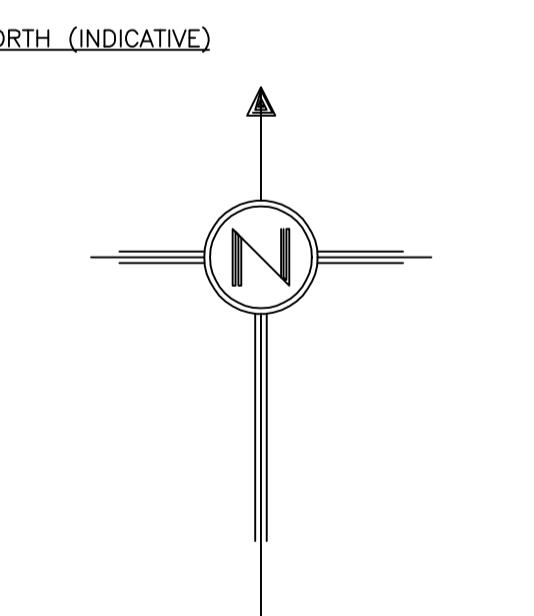
O	EMPTY BLOCK & BORDER
BTELCOM	BRITISH TELECOM MHS ETC.
BUILDING	BUILDING OUTLINE
CABIN	CABIN ROOFS
CONTOURS	CONTOURS
DRAINS	POND, GULLY'S ETC.
FOLIAGE	MASS, GULLY'S ETC.
GAS LINES	ELECTRIC, GAS MHS ETC.
GRID	FENCE LINES, GAS MHS/VALVES ETC.
LEVELS	GAS MHS/VALVES ETC.
ROADS	ROAD OUTLINE
STORM	STORM WATER MHS, GULLY'S ETC.
SURFACES	SURFACE EDGES
TREES	TREE OUTLINE & FOLIAGE
WALLS	UNOWNED SERVICES
WATER	WATER OUTLINE
WISERVICES	WATER METERS, STOP VALVES ETC.

LINETYPES & SYMBOLS

Building Outline
Kerb Line
Fence
Surface Edge
Foul Drainage
Storm Drainage
Gas Pipes
Water Service Pipes
British Telecom Cables
Electricity Cables
Overhead Cables
Foliage Outline
Survey Station
Gates
Tree Canopy
Slope Symbol

LEGEND

AV	AIR VALVE	NP	NAME PLATE
BB	BEACH BEACON	OB	OPEN BOARDED FENCE
BM	BUSS STOP MARK	OP	OPEN PALING FENCE
BTB	BRITISH TELECOM BOX	PC	POST & CHAIN FENCE
BW	BRITISH WATER BOX	PCB	POLICE CALL BOX
CB	CLOSE BOARD FENCE	PL	PAVEMENT LIGHT
CH	CORNER STONE	PN	PARKING INDICATOR
CHY	CHIMNEYS	PR	POST & RAIL FENCE
CI	COMMUNICATED IRON FENCE	PRF	POST & RAIL FENCE
CL	CHAIN LINK FENCE	PWM	POST & WIRE MESH
CM	CEMETERY	RS	ROAD SIDE
CTV	CABLE TELEVISION POINT	RTW	RETAINING WALL
DR	DRIVE CHANNEL	SV	STOP VALVE
DK	DROP KERB	TG	TELEGRAPH POLE
ELC	EMERGENCY LIGHT	TP	TELEGRAPH POLE
STN	EMERGENCY SUB STATION	UT	UNAVAILABLE TO LFT.
FP	FOOT BRIDGE	VP	VENT PIPE
FPH	FOOTPATH	WB	WASH BARRIER
FPJ	FLUXTHERM JACKET	WM	WATER METER
GR	GROVE	WO	WASH OUT
GZ	GAS VALVE		
H	HYDRAULIC		
IC	INSPECTION COVER		
IR	IRON RINGS		
KO	KERB OUTLET (GULLY)		
LB	LETTER BOX		
MSC	MINIMUM CONSTRUCTION FENCE		
MH	MANNHOLE		
MHE	MINIMUM TELECOM		
MHG	ELECTRICAL		
MHC	GAS		
MP	MERCURY		
NB	MILE POST		
	NOTICE BOARD		



LAND & MEASURED BUILDING SURVEYORS
M.J.ZARA ASSOCIATES
139 HIGH STREET - LEWES
EAST SUSSEX - BN7 1XS
TEL 01273 472492
E-MAIL: mizaraassociates@gmail.com

SITE
LAND AT THISTLEWORTH FARM, DIAL POST
WEST SUSSEX
CLIENT
MR A. HYATT
X-REF: DOUGLAS J.P.EDWARDS
NOTES
LEVELS AND GRID BASED ON ORDNANCE
SURVEY DATUM VIA GPS.
CONTOURS ARE COMPUTER GENERATED.
JOB REF. 9022 PREVIOUS JOB REF. 8814
SCALE 1:1000 SHEET SIZE A1 LANDSCAPE
DATE MAY 2020 SURVEYED BY EH/CS



Appendix C Infiltration Test Results

SOAKAWAY TEST RESULTS & SOILS INFILTRATION RATE

Site: Thistleworth Farm

Job No: D1867

Trial Hole: Hole A Test 1 of 2

Time in minutes	Depth in meters to water surface	Depth in metres of water	Percentage of water depth at start
0.00	0.000	0.40	100.0%
2.50	0.040	0.36	90.0%
5.00	0.060	0.34	85.0%
7.50	0.070	0.33	82.5%
10.00	0.080	0.32	80.0%
15.00	0.100	0.30	75.0%
20.00	0.120	0.28	70.0%
40.00	0.170	0.23	57.5%
60.00	0.210	0.19	47.5%
100.00	0.250	0.15	37.5%
160.00	0.300	0.10	25.0%
220.00	0.350	0.05	12.5%
310.00	0.400	0.00	0.0%
310.00	0.400	0.00	0.0%

INFILTRATION CALCULATED FROM 75%-25% WATER DEPTH RANGE

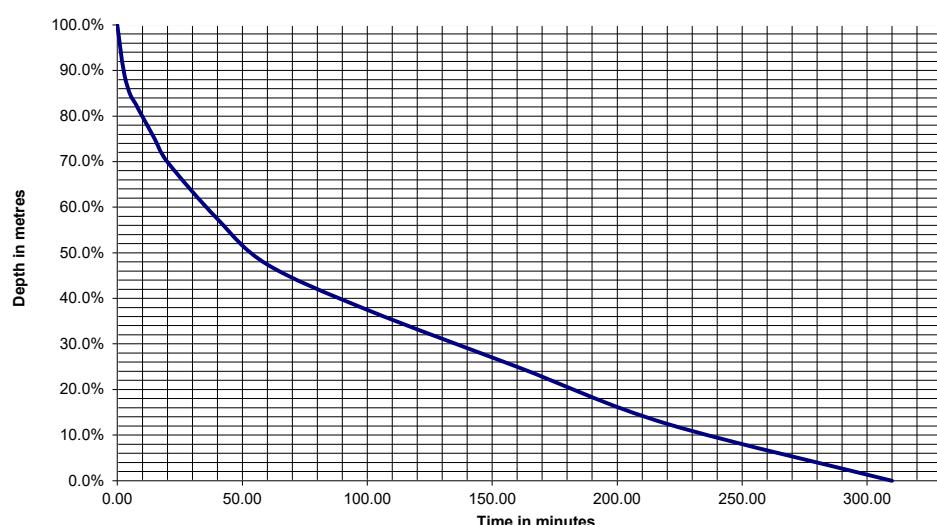
Pit Size	Time in mins
Length	15 75%
Width	160 25%
Depth	0.40

Infiltration Rate

from 75%-25%

1.04948E-05

Permeability Graph TH02



SOAKAWAY TEST RESULTS & SOILS INFILTRATION RATE

Site: Thistleworth Farm

Job No: D1867

Trial Hole: Hole A Test 2 of 2

Time in minutes	Depth in meters to water surface	Depth in metres of water	Percentage of water depth at start
0.00	0.000	0.45	100.0%
2.50	0.020	0.43	95.6%
5.00	0.030	0.42	93.3%
7.50	0.035	0.42	92.2%
10.00	0.040	0.41	91.1%
20.00	0.060	0.39	86.7%
30.00	0.090	0.36	80.0%
45.00	0.120	0.33	73.3%
60.00	0.150	0.30	66.7%
120.00	0.260	0.19	42.2%
180.00	0.340	0.11	24.4%
240.00	0.420	0.03	6.7%
300.00	0.450	0.00	0.0%
300.00	0.450	0.00	0.0%

INFILTRATION CALCULATED FROM 75%-25% WATER DEPTH RANGE

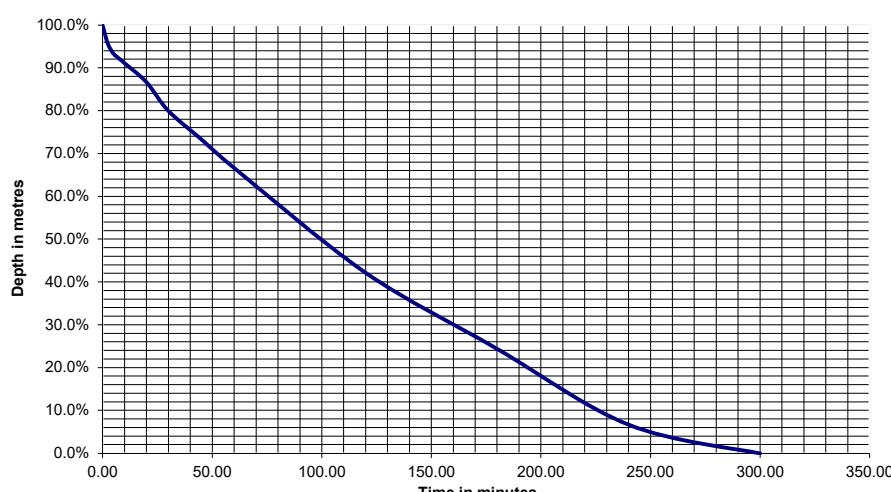
Pit Size	Time in mins
Length	42 75%
Width	175 25%
Depth	0.45

Infiltration Rate

from 75%-25%

1.2053E-05

Permeability Graph TH02



SOAKAWAY TEST RESULTS & SOILS INFILTRATION RATE

Site: Thistleworth Farm

Job No: D1867

Trial Hole: Hole B Test 1 of 1

Time in minutes	Depth in meters to water surface	Depth in metres of water	Percentage of water depth at start
0.00	0.000	0.45	100.0%
2.50	0.020	0.43	95.6%
5.00	0.030	0.42	93.3%
7.50	0.040	0.41	91.1%
10.00	0.045	0.41	90.0%
20.00	0.070	0.38	84.4%
40.00	0.100	0.35	77.8%
60.00	0.125	0.33	72.2%
120.00	0.225	0.23	50.0%
180.00	0.310	0.14	31.1%
240.00	0.370	0.08	17.8%
300.00	0.430	0.02	4.4%
300.00	0.430	0.02	4.4%

INFILTRATION CALCULATED FROM 75%-25% WATER DEPTH RANGE

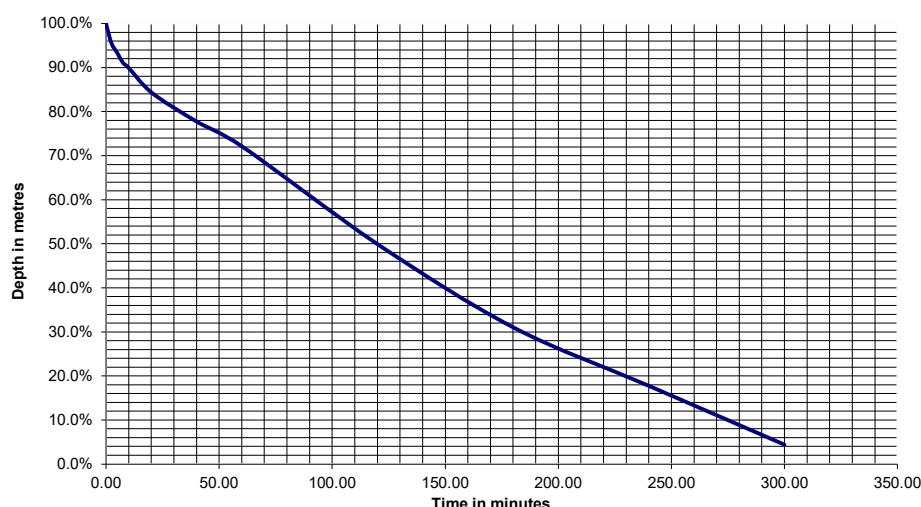
Pit Size	Time in mins
Length	50 75%
Width	212 25%
Depth	0.45

Infiltration Rate

from 75%-25%

9.70248E-06

Permeability Graph TH02





Appendix D BGS Records

1529.1893

GROUND LEVEL.....A.O.D.
 DATE STARTED.....27/2/1967
 DATE COMPLETED.....27/2/1967

TYPE OF BORING.....HAND AUGER.....
 DIA. OF BORING.....8.....ins.
 BOREHOLE LINED TO.....ft.....ins.

Geological Formation	Legend	Description of Strata	Depth	Samples	Water Levels	Geological Survey
WEALD CLAY	TOPSOIL		6"			British Geological Survey
		FIRM BROWN - GREY SILTY CLAY	1' 6"			
		FIRM GREY VERY SILTY CLAY	2' 6"			
		FIRM ORANGE-GREY SILTY CLAY	3' 6"			
		STIFF MOTTLED ORANGE AND GREY SILTY CLAY	8' 0"			
						British Geological Survey
						British Geological Survey
						British Geological Survey
						British Geological Survey
						British Geological Survey
REMARKS: British Geological Survey NO GROUNDWATER ENCOUNTERED			KEY:  WATER STRUCK  STANDING WATER LEVEL  UNDISTURBED SAMPLE  STANDARD PENETRATION TEST (23) NO OF BLOWS FOR 12" PENETRATION  SLIPPED CORE			
ORDER N°	6112	LABORATORY N°	2803		SCALE: 1 in. = 5 ft.	
SITE INVESTIGATION BY LE GRAND ADSCO		A24. DIAL POST DIVERSION FOR WEST SUSSEX COUNTY COUNCIL				

GROUND LEVEL A.O.D. TYPE OF BORING HAND AUGER
 DATE STARTED 28.2.1967 DIA. OF BORING 8 ins.
 DATE COMPLETED 11.3.1967 BOREHOLE LINED TO ft. ins.

Geological Formation	Legend	Description of Strata	Depth	Samples	Water Levels
WEALD CLAY		TOP SOIL			
		FIRM MOTTLED ORANGE-GREY SANDY SILTY CLAY			
		DITTO			
		FIRM TO STIFF MOTTLED GREY SILTY CLAY	8' 0"		
British Geological Survey		British Geological Survey			British Geological Survey
British Geological Survey		British Geological Survey			British Geological Survey
British Geological Survey		British Geological Survey			British Geological Survey
British Geological Survey		British Geological Survey			British Geological Survey
British Geological Survey		British Geological Survey			British Geological Survey

REMARKS:

British Geological Survey
NO GROUNDWATER ENCOUNTERED

KEY:

- WATER STRUCK
- STANDING WATER LEVEL
- UNDISTURBED SAMPLE
- STANDARD PENETRATION TEST
- (25) N of BLOWS FOR 12" PENETRATION
- SLIPPED CORE
- SCALE: 1h. = 5 ft.

ORDER NO. 6112

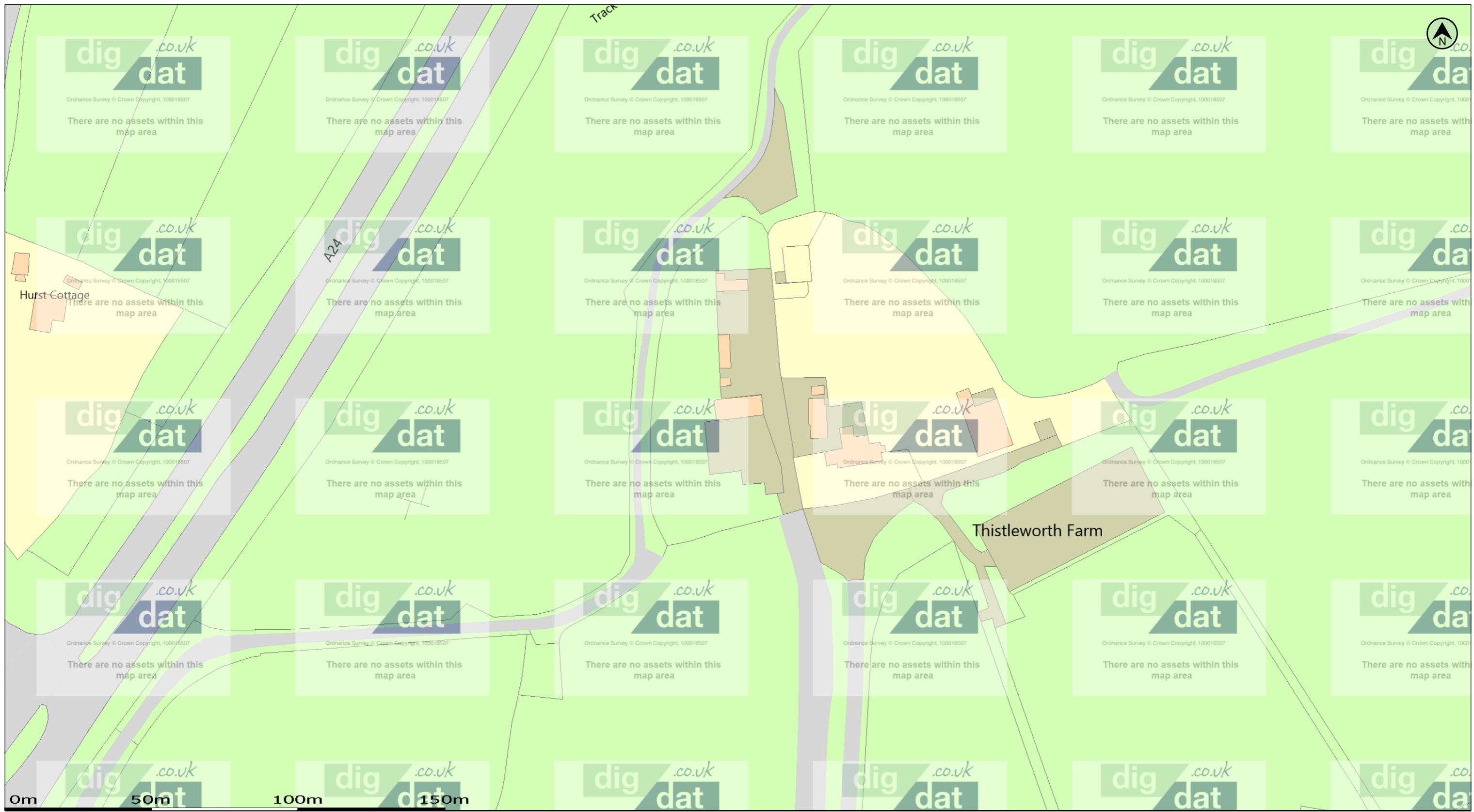
LABORATORY NO. 2803

SITE INVESTIGATION
BY
LE GRAND ADSCO

A24 DIAL POST DIVERSION
FOR
WEST SUSSEX COUNTY COUNCIL



Appendix E Southern Water Sewer Records



(c) Crown copyright and database rights 2020 Ordnance Survey 100031673

Date: 18/05/20

Scale: 1:1250

Map Centre: 515549,118953

Data updated: 01/04/20

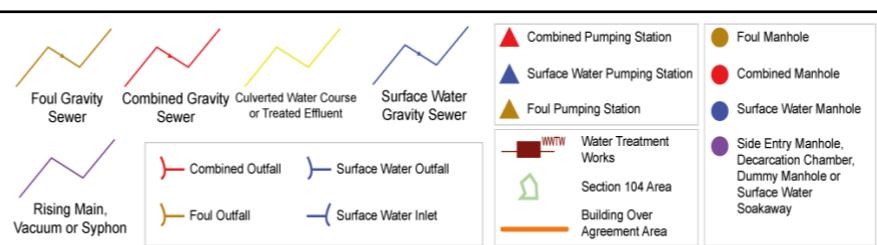
Our Ref: 389053 - 1

Wastewater Plan A3

The positions of pipes shown on this plan are believed to be correct, but Southern Water Services Ltd accept no responsibility in the event of inaccuracy. The actual positions should be determined on site. This plan is produced by Southern Water Services Ltd (c) Crown copyright and database rights 2020 Ordnance Survey 100031673 .This map is to be used for the purposes of viewing the location of Southern Water plant only. Any other uses of the map data or further copies is not permitted.

WARNING: BAC pipes are constructed of Bonded Asbestos Cement.

WARNING: Unknown (UNK) materials may include Bonded Asbestos Cement.



m.akmenkalns@bpcivils.co.uk
Thistleworth Farm



Manhole Reference	Liquid Type	Cover Level	Invert Level	Depth to Invert
-------------------	-------------	-------------	--------------	-----------------

Manhole Reference	Liquid Type	Cover Level	Invert Level	Depth to Invert
-------------------	-------------	-------------	--------------	-----------------

Manhole Reference	Liquid Type	Cover Level	Invert Level	Depth to Invert
-------------------	-------------	-------------	--------------	-----------------



Appendix F Drainage Calculations

Calculated by:	Daniel Lytton
Site name:	Thistleworth Farm
Site location:	RH13 8NR

This is an estimation of the greenfield runoff rates that are used to meet normal best practice criteria in line with Environment Agency guidance "Rainfall runoff management for developments", SC030219 (2013) , the SuDS Manual C753 (Ciria, 2015) and the non-statutory standards for SuDS (Defra, 2015). This information on greenfield runoff rates may be the basis for setting consents for the drainage of surface water runoff from sites.

Site Details

Latitude:	50.95842° N
Longitude:	0.35773° W
Reference:	1320379454
Date:	May 26 2020 10:11

Runoff estimation approach

IH124

Site characteristics

Total site area (ha):

1.9

Notes

(1) Is $Q_{BAR} < 2.0 \text{ l/s/ha}$?

When Q_{BAR} is $< 2.0 \text{ l/s/ha}$ then limiting discharge rates are set at 2.0 l/s/ha .

Methodology

Q_{BAR} estimation method:

Calculate from SPR and SAAR

SPR estimation method:

Calculate from SOIL type

Soil characteristics

SOIL type:

Default	Edited
4	4
N/A	N/A
0.47	0.47

HOST class:

SPR/SPRHOST:

Hydrological characteristics

SAAR (mm):

Default	Edited
810	810
7	7
0.85	0.85
2.3	2.3
3.19	3.19
3.74	3.74

Hydrological region:

Growth curve factor 1 year:

Growth curve factor 30 years:

Growth curve factor 100 years:

Growth curve factor 200 years:

(2) Are flow rates $< 5.0 \text{ l/s}$?

Where flow rates are less than 5.0 l/s consent for discharge is usually set at 5.0 l/s if blockage from vegetation and other materials is possible. Lower consent flow rates may be set where the blockage risk is addressed by using appropriate drainage elements.

(3) Is $SPR/SPRHOST \leq 0.3$?

Where groundwater levels are low enough the use of soakaways to avoid discharge offsite would normally be preferred for disposal of surface water runoff.

Greenfield runoff rates

Default	Edited
10.88	10.88
9.25	9.25
25.03	25.03
34.71	34.71
40.7	40.7

This report was produced using the greenfield runoff tool developed by HR Wallingford and available at www.ukuds.com. The use of this tool is subject to the UK SuDS terms and conditions and licence agreement , which can both be found at www.ukuds.com/terms-and-conditions.htm. The outputs from this tool are estimates of greenfield runoff rates. The use of these results is the responsibility of the users of this tool. No liability will be accepted by HR Wallingford, the Environment Agency, CEH, Hydrosolutions or any other organisation for the use of this data in the design or operational characteristics of any drainage scheme.



Bright Plan Civils
2 West Barn
Norton Lane
Chichester PO20 3AF

File: D1867 Drainage Design.pfd
Network: Storm Network
Dan Lytton
12/06/2020

Page 1
Thistleworth Farm
Dial Post RH13 8NR
Catchment Drainage Strategy

Design Settings

Rainfall Methodology	FSR	Maximum Time of Concentration (mins)	30.00
Return Period (years)	2	Maximum Rainfall (mm/hr)	250.0
Additional Flow (%)	10	Minimum Velocity (m/s)	1.00
FSR Region	England and Wales	Connection Type	Level Soffits
M5-60 (mm)	20.000	Minimum Backdrop Height (m)	0.200
Ratio-R	0.300	Preferred Cover Depth (m)	0.600
CV	1.000	Include Intermediate Ground	✓
Time of Entry (mins)	5.00	Enforce best practice design rules	✓

Nodes

	Name	Area (ha)	T of E (mins)	Cover Level	Diameter (mm)	Depth (m)
	1	0.349	5.00	29.000	1200	1.200
	2		5.00	29.000	1200	1.000
	3			28.500	1200	1.200
	4			28.500	1200	1.300

Links

Name	US Node	DS Node	Length (m)	ks (mm) / n	US IL (m)	DS IL (m)	Fall (m)	Slope (1:X)	Dia (mm)	T of C (mins)	Rain (mm/hr)
1.01	1	3	15.000	0.600	27.800	27.500	0.300	50.0	225	5.13	60.0
2.01	2	3	10.000	0.600	28.000	27.625	0.375	26.7	100	5.11	60.1
3.01	3	4	6.500	0.600	27.300	27.200	0.100	65.0	225	5.20	59.7

Name	Vel (m/s)	Cap (l/s)	Flow (l/s)	US Depth (m)	DS Depth (m)	Σ Area (ha)	Σ Add Inflow (l/s)
1.01	1.854	73.7	83.2	0.975	0.775	0.349	0.0
2.01	1.500	11.8	0.0	0.900	0.775	0.000	0.0
3.01	1.624	64.6	82.8	0.975	1.075	0.349	0.0

Simulation Settings

Rainfall Methodology	FSR	Drain Down Time (mins)	240
FSR Region	England and Wales	Additional Storage (m³/ha)	20.0
M5-60 (mm)	20.000	Check Discharge Rate(s)	✓
Ratio-R	0.300	1 year (l/s)	9.3
Summer CV	1.000	30 year (l/s)	26.1
Winter CV	1.000	100 year (l/s)	34.7
Analysis Speed	Normal	Check Discharge Volume	✓
Skip Steady State	x	100 year +40% 360 minute (m³)	1001

Storm Durations

15 | 30 | 60 | 120 | 180 | 240 | 360 | 480 | 600 | 720 | 960 | 1440

Return Period (years)	Climate Change (CC %)	Additional Area (A %)	Additional Flow (Q %)
100	40	0	0



Bright Plan Civils
2 West Barn
Norton Lane
Chichester PO20 3AF

File: D1867 Drainage Design.pfd
Network: Storm Network
Dan Lytton
12/06/2020

Page 2
Thistleworth Farm
Dial Post RH13 8NR
Catchment Drainage Strategy

Pre-development Discharge Rate

Site Makeup	Greenfield	Growth Factor 30 years	2.40
Greenfield Method	IH124	Growth Factor 100 years	3.19
Positively Drained Area (ha)	1.900	Betterment (%)	0
SAAR (mm)	810	QBar	10.9
Soil Index	4	Q 1 year (l/s)	9.3
SPR	0.47	Q 30 year (l/s)	26.1
Region	7	Q 100 year (l/s)	34.7
Growth Factor 1 year	0.85		

Pre-development Discharge Volume

Site Makeup	Greenfield	Return Period (years)	100
Greenfield Method	FSR/FEH	Climate Change (%)	40
Positively Drained Area (ha)	1.900	Storm Duration (mins)	360
Soil Index	4	Betterment (%)	0
SPR	0.47	PR	0.538
CWI	121.482	Runoff Volume (m³)	1001

Node 2 Time-Area Diagram

Overrides Design Area	x	Depression Storage Depth (mm)	10
Overrides Design Additional Inflow	x	Evapo-transpiration (mm/day)	10
Depression Storage Area (m²)	10000		

Applies to All storms

Time	Area	Time	Area	Time	Area	Time	Area	Time	Area
(mins)	(ha)	(mins)	(ha)	(mins)	(ha)	(mins)	(ha)	(mins)	(ha)
0-60	0.060	60-120	0.060	120-180	0.060	180-240	0.060	240-300	0.060

Node 3 Online Hydro-Brake® Control

Flap Valve	x	Objective	(HE) Minimise upstream storage
Replaces Downstream Link	✓	Sump Available	✓
Invert Level (m)	27.300	Product Number	CTL-SHE-0132-8000-1000-8000
Design Depth (m)	1.000	Min Outlet Diameter (m)	0.150
Design Flow (l/s)	8.0	Min Node Diameter (mm)	1200

Node 1 Depth/Area Storage Structure

Base Inf Coefficient (m/hr)	0.00000	Safety Factor	1.0	Invert Level (m)	27.800
Side Inf Coefficient (m/hr)	0.00000	Porosity	0.32	Time to half empty (mins)	10

Depth	Area	Inf Area	Depth	Area	Inf Area
(m)	(m²)	(m²)	(m)	(m²)	(m²)
0.000	104.0	0.0	1.200	104.0	0.0

Node 3 Depth/Area Storage Structure

Base Inf Coefficient (m/hr)	0.00000	Safety Factor	1.0	Invert Level (m)	27.300
Side Inf Coefficient (m/hr)	0.00000	Porosity	1.00	Time to half empty (mins)	

Depth	Area	Inf Area	Depth	Area	Inf Area
(m)	(m²)	(m²)	(m)	(m²)	(m²)
0.000	120.0	0.0	1.200	385.0	0.0



Approval Settings

Node Size	✓	Maximum Full Bore Velocity (m/s)	3.000
Node Losses	✓	Proportional Velocity	✓
Link Size	✓	Return Period (years)	
Minimum Diameter (mm)	150	Minimum Proportional Velocity (m/s)	0.750
Link Length	✓	Maximum Proportional Velocity (m/s)	3.000
Maximum Length (m)	100.000	Surcharged Depth	✓
Coordinates	✓	Return Period (years)	
Accuracy (m)	1.000	Maximum Surcharged Depth (m)	0.100
Crossings	✓	Flooding	✓
Cover Depth	✓	Return Period (years)	30
Minimum Cover Depth (m)		Time to Half Empty	x
Maximum Cover Depth (m)	3.000	Discharge Rates	✓
Backdrops	✓	1 year (l/s)	
Minimum Backdrop Height (m)		30 year (l/s)	
Maximum Backdrop Height (m)	1.500	100 year (l/s)	
Full Bore Velocity	✓	Discharge Volume	✓
Minimum Full Bore Velocity (m/s)		100 year 360 minute (m³)	

Rainfall

Event	Peak Intensity (mm/hr)	Average Intensity (mm/hr)	Event	Peak Intensity (mm/hr)	Average Intensity (mm/hr)
100 year +40% CC 15 minute summer	441.486	124.925	100 year +40% CC 360 minute summer	63.377	16.309
100 year +40% CC 15 minute winter	309.815	124.925	100 year +40% CC 360 minute winter	41.197	16.309
100 year +40% CC 30 minute summer	304.460	86.152	100 year +40% CC 480 minute summer	50.006	13.215
100 year +40% CC 30 minute winter	213.656	86.152	100 year +40% CC 480 minute winter	33.223	13.215
100 year +40% CC 60 minute summer	214.603	56.713	100 year +40% CC 600 minute summer	40.997	11.214
100 year +40% CC 60 minute winter	142.577	56.713	100 year +40% CC 600 minute winter	28.011	11.214
100 year +40% CC 120 minute summer	135.791	35.885	100 year +40% CC 720 minute summer	36.560	9.799
100 year +40% CC 120 minute winter	90.216	35.885	100 year +40% CC 720 minute winter	24.571	9.799
100 year +40% CC 180 minute summer	104.615	26.921	100 year +40% CC 960 minute summer	30.041	7.911
100 year +40% CC 180 minute winter	68.003	26.921	100 year +40% CC 960 minute winter	19.900	7.911
100 year +40% CC 240 minute summer	82.776	21.875	100 year +40% CC 1440 minute summer	21.775	5.836
100 year +40% CC 240 minute winter	54.994	21.875	100 year +40% CC 1440 minute winter	14.634	5.836



Results for 100 year +40% CC Critical Storm Duration. Lowest mass balance: 99.93%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m³)	Flood (m³)	Status
30 minute summer	1	21	28.993	1.192	237.6	47.9718	0.0000	FLOOD RISK
480 minute summer	2	464	28.982	0.982	14.0	7.0009	0.0000	FLOOD RISK
720 minute summer	3	705	28.458	1.158	34.5	288.2105	0.0000	FLOOD RISK
15 minute summer	4	1	27.200	0.000	8.0	0.0000	0.0000	OK

Link Event (Upstream Depth)	US Node	Link Node	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m³)	Discharge Vol (m³)
30 minute summer	1	1.01	3	133.1	3.347	1.806	0.5966	
480 minute summer	2	2.01	3	13.8	1.761	1.169	0.0782	
720 minute summer	3	Hydro-Brake®	4	8.6				382.7