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Flood Risk Assessment & Surface Water Drainage Assessment

June 2023

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Hooklands Farm London Road Ashington West Sussex RH20 3AT

JBA Project Manager

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Contract

This report describes work commissioned by Mark Nunn, on behalf of Penfold Verrall Ltd. Dimitrios Goukos of JBA Consulting carried out this work.

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Purpose

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1 Introduction

1.1 Overview

This proportionate Flood Risk Assessment (FRA) and Surface Water Drainage Assessment (SWDA) has been prepared following instruction from Mark Nunn, on behalf of Penfold Verrall Ltd, by an email dated 17/04/2023. The development was for the Hooklands Farmhouse noise, air quality and light pollution mitigation scheme. They will provide support for the required land raising proposals that will allow the validation of the original 'Application for Planning Permission' prepared by Ashdown Planning Consultants.

This FRA and SWDA is based on a desktop review of the proposed development layout.

1.2 Scope

The proposed land raising scheme is located at Hooklands Farmhouse, shown on Figure 2-1. A planning application has already been submitted. However, this application has not been validated due to the request for further detailed information on issues relevant to flooding and drainage by West Sussex County Council (WSCC).

Penfold Verrall wish to secure a valid planning application, and so want to address these outstanding validation issues by commissioning this additional assessment.

2 Spatial Planning Considerations

2.1 Location

The proposed development is located in Hooklands Farm, London Road, Ashington, West Sussex, RH20 3AT (see Figure 2-1 and Table 2-1 below).

The site lies within the Lancing Brook catchment that joins River Adur near Knepp Castle, about 3.5 Km north of the development, while, to the south (around 1.2 Km) lies the large village of Ashington.

Table 2-1: Location of the Development Site

Reference	Value
OS X (Eastings)	513476
OS Y (Northings)	116910
Nearest Post Code	RH20 3AT
Lat (WGS84)	N50:56:26
Long (WGS84)	W0:23:11
Nat. Grid	TQ134 <mark>169</mark>

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Figure 2-1: Wider Location Plan

2.2 Pre and Post Development Site Description

The development site covers approximately 4.5 hectares and consists predominately of grassland, a hardstanding access track, and surrounding deciduous woodland. The wider landscape is comprised of agricultural land and woodland parcels with hedgerows and treelines.

The development involves land raising towards the A24 in order to create two bunds that will mitigate noise, air quality and light pollution. A temporary haul road will provide access for the erection of these two bunds (Figure 2-2). A site compound and parking of vehicles for site operatives and visitors will also be established (Figure 2-3). It will contain a standalone 12ft welfare unit that provides facilities up to 7 site operatives.

The temporary haul road is proposed to pass through fields to the west of Hooklands Farm and link into the existing old A24 road next to No 2 Hooklands Lodge (Figure 2-2).

Also, a wheel cleaning facilities area will be established at the entrance to the site to ensure no debris is deposited onto the highway (Figure 2-3). All vehicles leaving the site will use this facility.

The aforementioned will all be removed upon completion of the works.

The existing and proposed site development layouts are presented in Figure 2-2 (red contours: existing terrain / blue contours: terrain after the intervention). Figure 2-2 indicates where the developer is proposing to construct the two, parallel with A24, bunds. The amounts proposed are a maximum of circa 110,000 cubic metres.





Figure 2-2: Existing and Proposed Site Layout (with temporary haul road)



Figure 2-3: Site Compound, Parking and Wheel Cleaning Facilities Area



2.3 Topography – Local Hydrological Network

The existing ground elevations on site is shown in Figure 2-4 (yellow contours). It indicates that the site is split by the existing access road to a western side, sloping towards the north west of the site's boundary (see below Section 2.6.1), and specifically the existing pond, and an eastern side, sloping towards the north eastern corner of the site, where the parallel to the site's boundary drainage ditch (indicated by the characteristic folds alongside the eastern boundary) also ends up (see below Section 2.6.1). Ground levels vary between 45mAOD and 34mAOD.



Figure 2-4: Pre-development topography (Yellow contours)

The post-development ground elevations on site is shown in Figure 2-5 (blue contours). It indicates that the topographical alteration will cause a respective modification in the hydromorphic characteristics of the site (see below Section 2.6.1).

Ground levels will vary between 48.5mAOD and 34mAOD.



Figure 2-5: Post-development topography (purple contours)

Figure 2-6 depicts the local hydrological network. We can see that both north west and north east corners of our site are the starting points of two brooks, merging downstream before they end up in Lancing Brook. The one in the west side flows out of the aforementioned pond.

These two local brooks are the receptors of the surface water runoff occurring from our site.

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Figure 2-6: Local Hydrological Network

2.4 Soil conditions - Infiltration rate

Soilscapes mapping provided by Cranfield University on behalf of DEFRA (Figure 2-7) shows that the site of the proposed development falls on HOST soil class 18, which is defined as 'Slowly permeable seasonally wet slightly acid but base-rich loamy and clayey soils'.

Information from the Soilscapes mapping suggests that the specific soils may be suitable for the use of SuDS methods, concerning surface water runoff handling, involving infiltration.

In dry soil, water infiltrates rapidly. This is called the initial infiltration rate. As more water replaces the air in the pores, the water from the soil surface infiltrates more slowly and eventually reaches a steady rate. This is called the basic infiltration rate.

Soilscapes refers the site's soil texture as 'loamy and clayey'. According to FAO's 'Irrigation Water Management: Irrigation methods' the basic infiltration rates, for this type of soil, vary between 5 and 10mm/h. We will accept, in the lack of field evidence (infiltration test) that an average value of 7.5mm/h is representative for the site.





Figure 2-7: Cranfield University Soilscapes mapping

2.5 Runoff Coefficient

The runoff coefficient (Cv) is a dimensionless coefficient relating the amount of runoff to the amount of precipitation received. Agricultural land's runoff coefficient, and specifically, grassland and pasture growing on a 'loamy and clayey' soil, according to the literature, varies between 0.1 and 0.4. We will accept that an average value of 0.25 is representative for the site.

2.6 Pre, during and post development drainage patterns

The determination of how the intervention will impact (increase) flooding risk (from surface water runoff) within its boundary or downstream, depends on the changes that will occur in the drainage patterns, and specifically:

- terrain alterations (changes in hydromorphic characteristics due to changes in topography)
- infiltration patterns changes

2.6.1 Topography related impact

The erection of the bund will redistribute surface water flowpaths as shown in Figure 2-8.

Initially surface water was flowing fairly uniformly towards the lower points of the two distinct drainage parts, as described in Section 2.3. The intervention will change the pattern of runoff as water will flow in a perimetric way around each bund (Figure 2-8).

This means that surface water will flow towards the existing access road from both 'eastern' and 'western' bund (Figure 2-8), while, before the intervention water could only move towards the aforementioned receptors.



In addition, surface water will be conveyed southerly from the south-sloping sides of each bund, towards the areas neighbouring A24 (Figure 2-8) where it may create pool(s) of stagnant water.

This redistribution will need to be mitigated (see below Section 4.2) in order to avoid erosion phenomena both to the access road and the toe of the bunds themselves.

In conclusion, there will be an increase in flood risk, during and post the intervention, because of the obvious terrain alteration, which will respectively cause changes in the hydromorphic characteristics. As a mitigation we will propose in Section 4.2 a drainage arrangement capable of it.



Figure 2-8: Pre and post development flowpaths

2.6.2 Infiltration patterns related impact

The erection of the two bunds, the temporary haul road, the site compound (and parking) and the wheel cleaning facilities area will not change the infiltration patterns of the site. According to the 'Construction Management Plan' by Penfold Verrall, submitted with the original 'Application for Planning Permission':

- The material to be deposited at the site will be clean naturally occurring soil and mineral material and will be imported according to a Materials Management Plan (MMP) under the Definition of Waste: Code of Practice (DoWCoP / CL:AIRE) which regulates/enables the direct transfer and reuse of clean naturally occurring soil materials between sites.
- The temporary haul road will consist of a stoned track built to specifications to match the lorry weights required to minimise ground compaction. It will be constructed from recycled stone and enabling lorries to access the working area safely. The track would be 4 metres wide with passing bays incorporated to allow safe passing of on-site traffic and will be located outside of any tree root protection areas. The existing topsoil would be stripped and stored separately to a height of 2.0m and also outside the tree root protection areas. The track will be removed once the site operations have been completed prior to re-spreading the topsoil. Vehicular movements during the construction period shall be limited



to areas of existing and new temporary hard standing or newly protected ground only.

- The site compound and parking will be established by laying a geotextile membrane to the existing ground and laying a recycled stone upon this and consolidating.
- The wheel cleaning facilities area will occupy part of the temporary haul road. Any washwater is in the responsibility of the contractor to manage.

It is considered that there will be no increase in flood risk during and post the intervention due to infiltration patterns' alteration as, according to the above, they will not change.

It is for the contractor that will erect the bunds to handle any washwater in order to avoid contamination issues.

3 Flood Risk

The site, as will be shown below, is at very low flood risk from fluvial, pluvial, sewer and artificial flood sources (reservoirs).

No tidal and groundwater assessment has been performed as they were regarded improbable eventualities.

3.1 Fluvial Flooding

The site is within 'Flood Zone 1', defined as areas having less than 1 in 1,000 annual exceedance probability of river flooding (Figure 3-1), therefore it is at very low fluvial flood risk.



Figure 3-1: Flood Zones (Source: EA Flood Map for Planning)



3.2 Sequential Test/Exception Test - NPPF Vulnerability

No Sequential Test/Exception Test will be required as the site lies in Flood Zone 1.

You need to do a sequential test if both of the following apply:

- The site is in flood zone 2 or 3
- A sequential test hasn't already been done for a development of the type you an plan to carry out on your proposed site

An exception test is required when the sequential test has been passed.

The development will be classed as 'Water-compatible development' under the NPPF vulnerability classification (Table 3-1). The flood risk vulnerability and flood zone compatibility are displayed in Table 3-2.

Table 3-1: Flood Risk Vulnerability Classification (Source: NPPF Technical Guide)

Water-compatible development
Flood control infrastructure.
Water transmission infrastructure and pumping stations.
Sewage transmission infrastructure and pumping stations.
Sand and gravel working.
Docks, marinas and wharves.
Navigation facilities.
Ministry of Defence installations.
Ship building, repairing and dismantling, dockside fish processing and refrigeration and compatible activities requiring a waterside location.
Water-based recreation (excluding sleeping accommodation).
Lifeguard and coastguard stations.
Amenity open space, nature conservation and biodiversity, outdoor sports and recreation and essential facilities such as changing rooms.
Essential ancillary sleeping or residential accommodation for staff required by uses in this category, subject to a specific warning and evacuation plan.

Table 3-2: Flood Risk Vulnerability and flood zone compatibility (Source: NPPF Technical Guide)

Flood Zones	Flood Risk Vulnerability Classification								
	Essential infrastructure	Highly vulnerable	More vulnerable	Less vulnerable	Water compatible				
Zone 1	1	1	1	1	1				
Zone 2	1	Exception Test required	1	1	1				
Zone 3a †	Exception Test required †	×	Exception Test required	1	1				
Zone 3b *	Exception Test required *	×	×	×	✓*				

Key:

✓ Development is appropriate

X Development should not be permitted.

As the development's closest category is 'Sand and gravel working' (Water-compatible) and it is located in Flood Zone 1 the development is acceptable; it is appropriate to proceed with it.

3.3 Flood Compensation Storage

No flood compensation storage will be required as the site is lacated in Flood Zone 1.

3.4 Flooding from Artificial Sources

Based on the Environment Agency's Flood Risk mapping (Figure 3-2), the proposed development is located entirely outside reservoir flood extents.



Maximum extent of flooding from reservoirs:

🔵 when river levels are normal 🥘 when there is also flooding from rivers 🛛 🕁 Location you selected

Figure 3-2: Flood Extent from Reservoirs

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3.5 Surface Water Flooding

The Environment Agency Risk of Flooding from Surface Water (RoFSW) map is presented in Figure 3-3. The site is shown to be at very low risk of surface water flooding. Very low risk means that each year this area has a chance of flooding of less than 0.1%.

Surface water flood risk at the site appears to vary in a very small proportion of the total area while the vast majority remains at very low risk. These isolated areas shown to be at high risk likely are due to local depressions in topography.

It is important to stress that no overlay occurs between the none of the two bunds, the temporary haul road, the site compound (and parking) and the wheel cleaning facilities area, and the areas of surface water flood risk.





● <u>High</u> ● <u>Medium</u> ● <u>Low</u> ○ <u>Very low</u> ◆ Location you selected

Figure 3-3: Surface Water Flood Map

3.6 Flooding from Sewers

There are no existing sewers in the vicinity of the site.



4 Surface water drainage strategy

4.1 Overview of drainage strategy

The Surface Water Drainage Strategy (SWDS) includes the provision of SuDS, in order to manage the new hydromorphic situation created by the intervention, concerning runoff in the development site. As detailed in Section 2.4 infiltration is feasible at this site.

The idea behind the proposed drainage strategy is to dispose, utilising infiltration, the redistributed by the intervention, quantities of surface water, while allowing those that remain intact to follow their usual path to either of the two drainage routes shown in Figure 2-6.

After further investigation, it was considered that the most suitable option for managing surface water runoff would be the construction of perimetric swales around the bunds. Swales that will be capable of storing initially the surface water runoff quantities before they allow them to infiltrate.

The design event that was considered was the 100 year rainfall event plus 20% climate change allowance.

The climate change allowance was set to 20% after consulting the relevant Department for Environment Food & Rural Affairs Climate Change Allowances site ('Adur and Ouse Management Catchment peak rainfall allowances').

4.2 **Positioning and sizing of the swales**

The SWDS will rely on the targeted attenuation (storage) of the unfavourably redistributed runoff and its disposal through infiltration (Section 2.6.1). Figure 4-1 shows the areas requiring drainage and the respective positioning of the proposed swales. Swale East 1, Swale East 2, Swale West 1 and Swale West 2 are the areas requiring drainage. No alteration in the drainage patterns have been regarded for the rest of the site's areas.

Modelling of the surface water runoff to the design parameters was carried out using the Source Control of Micro Drainage, an industry leading software which allows design and analysis of SuDS features. Original model results are displayed in Appendix A: MicroDrainage-Source Control Results. The following conservative assumptions and design parameters have been set within the Hydraulic model:

- Swale East 1, Swale East 2, Swale West 1 and Swale West 2 equal 0.323ha, 0.313ha, 1.418 and 0.399;
- Time take for runoff to reach the detention basin respectively has been set at 4 minutes (this takes into account the fact that impermeable surfaces are lying in a wide range of distance from the swale);
- Rainfall intensity was obtained using the FEH rainfall runoff methods and specifically the ReFH2 methodology (ReFH2 Tool), and increased by 20%, the central end allowance for climate change over the 30 years design life of the proposed site, in line with the requirements of the NPPF;
- No runoff loses have been assumed in the modelling, therefore all the design rainfall landing on the impermeable surfaces is expected to reach the swales;
- The dimensions of the detention basin are displayed in Appendix A: MicroDrainage-Source Control Results;
- As per the conclusions in Section 3.3, the soil has been modelled with an infiltration rate of 7.5 mm/hr;
- Runoff Coefficient was set to a value of 0.25.



Table 3 below includes a summary of the swales specifications, designed to collect and manage the rainfall runoff from the 1 in 100 year event plus climate change allowance. The SWDS plan showing the indicative layout of the swales and inflowing drainage areas, is displayed in Figure 4-1.

Table 4-1, below, includes a summary of swales' drainage areas, dimensions and performances for the 100 year rainfall event (plus 20% Climate Change Allowance).

Swale	Drained	Total	Depth (m)	Base	Side Slope	u/s ground	d/s ground	S/W Volume to be	Critical Storm Event	Half Drain	Max Depth
Swale	Area (m2)	Length (m)	Depth (III)	Width (m)	(1/X)	Level (mAOD)	Level (mAOD)	accomodated (m3)	Duration (min) - Season	Time (min)	(mm)
1	3,230	90	0.9	1.0	1/3	44.00	43.00	75	2160 Winter	2,861	800
2	3,130	98	1.3	1.0	1/3	44.50	40.75	79	2880 Winter	4,345	1,298
3	14,180	270	1.2	1.0	1/3	43.50	38.00	354	2880 Winter	4,126	1,184
4	3,990	115	1.1	1.0	1/3	44.00	41.75	98	2880 Winter	3,789	1,096

Table 4-1: Swales' drainage areas, dimensions and performance



Figure 4-1: Surface water drainage strategy layout



5 Conclusions

- The proposed development site is located in Hooklands Farm, London Road, Ashington, West Sussex, RH20 3AT (OS X (Eastings) 513476 / OS Y (Northings) 116910);
- The development involves the erection of two bunds towards A24 that will mitigate noise, air quality and light pollution.;
- This FRA is based on a desktop review of the proposed development layout;
- The proposed development site sits within Flood Zone 1. It is at very low flood risk from fluvial, pluvial, sewer and artificial flood sources (reservoirs);
- The development is considered as 'Water Compatible' according to the NPPF 'Flood Risk Vulnerability Classification';
- According to NPPF 'Flood Risk Vulnerability and Flood Zone Compatibility' there is no need of sequential and exception test, to determine whether the development is acceptable; it is appropriate to proceed with it;
- It is important to stress that no overlay occurs between the two bunds, the temporary haul road, the site compound (and parking) and the wheel cleaning facilities area, and the areas of fluvial or surface water flood risk;
- There will be an increase in flood risk, during and post the intervention, because of the obvious terrain alteration, which will respectively cause changes in the hydromorphic characteristics. A drainage arrangement (surface water drainage strategy) capable of mitigating these issues is proposed;
- The surface water drainage strategy comprises swales to dispose, utilising infiltration, the redistributed by the intervention, quantities of surface water, while allowing those that remain intact to follow their usual path to either of the two final receptors. Four swales will be required;
- The bunds, the temporary haul road, the site compound (and parking) and the wheel cleaning facilities area will not alter the hydromorphic characteristics of the site as they will be permeable structures;
- It is for the contractor that will erect the bunds to handle any washwater in order to avoid contamination issues.



Appendix A: MicroDrainage-Source Control Results

Swale East 1

e Library						
Philips Courty	ard					
leshill B46 3A						
				1 1 1 61	1	
te 06/06/2023 1				d by jflo	ow_athe	erstone
le 2023s0670 pr	oject_eas	• • • •	Checked	by		
cro Drainage			Source (Control 2	2020.1	.3
Summa	ry of Resi	ults f	or 100 y	ear Retu	rn Per	iod (+20%)
	На	lf Drai	in Time :	2861 minut	les.	
	Storm	Max	Max	Max	Max	Status
	Event		Depth Inf			
	Licito	(m)	(m)		(m ³)	
	min Summer				23.7	O K
30	min Summer	0.572	0.572	0.2	31.5	0 K
60	min Summer	0.627	0.627	0.2	39.9	Flood Risk
120	min Summer	0.676	0.676	0.2	48.4	Flood Risk
180	min Summer	0.702	0.702	0.2	53.2	Flood Risk
240	min Summer	0.718	0.718	0.2	56.5	Flood Risk
360	min Summer	0.741	0.741	0.2	61.2	Flood Risk
480	min Summer	0.756	0.756	0.2	64.5	Flood Risk
600	min Summer	0.766	0.766	0.2	66.9	Flood Risk
720	min Summer	0.705	0.705	0.3	58.7	riood Risk
960	min Summer	0.785	0.785	0.3	72.6	Flood Risk
2160	min Summer	0.795	0.795	0.3	73.0	Flood Risk
2880	min Summer	0.797	0.797	0.3	74.2	Flood Risk
4320	min Summer	0.793	0.793	0.3	73.2	Flood Risk
5760	min Summer	0.787	0.787	0.3	71.6	Flood Risk
7200	min Summer	0.779	0.779	0.3	69.8	Flood Risk
8640	min Summer	0.771	0.771	0.3	68.0	Flood Risk
10080	min Summer	0.762	0.762	0.2	66.1	Flood Risk
15	min Summer min Summer	0.510	0.510	0.1	23.7	0 K
	St	orm	Rain			ak
			1101111	Flooded	Time-Pe	
	Ev	ent		Volume		
	Ev	ent				
			(mm/hr)	Volume (m³)	(mins)	
			(mm/hr)	Volume (m³)	(mins)	
			(mm/hr)	Volume (m³)	(mins)	19
			(mm/hr)	Volume (m³)	(mins)	19 34
			(mm/hr)	Volume (m³)	(mins)	19 34 64 24
	15 m: 30 m: 60 m: 120 m: 180 m: 240 m:	.n Summ .n Summ .n Summ .n Summ .n Summ	(mm/hr) er 117.607 er 78.466 er 49.857 er 30.521 er 22.540 er 18.079	Volume (m ³) 0.0 0.0 0.0 0.0 0.0	(mins) 1 1 2	19 34 64 24 84
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	15 m: 30 m: 60 m: 120 m: 180 m: 240 m:	.n Summ .n Summ .n Summ .n Summ .n Summ	(mm/hr) er 117.607 er 78.466 er 49.857 er 30.521 er 22.540 er 18.079	Volume (m ³) 0.0 0.0 0.0 0.0 0.0	(mins) 1 1 2	19 34 64 24 84 44 64 82 02
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	15 m: 30 m: 60 m: 120 m: 180 m: 240 m:	.n Summ .n Summ .n Summ .n Summ .n Summ	(mm/hr) er 117.607 er 78.466 er 49.857 er 30.521 er 22.540 er 18.079	Volume (m ³) 0.0 0.0 0.0 0.0 0.0	(mins) 1 1 2	19 34 64 24 84 44 64 82 02 22 62 40 68 08 68 12
	15 m: 30 m: 60 m: 120 m: 180 m: 240 m:	.n Summ .n Summ .n Summ .n Summ .n Summ	(mm/hr) er 117.607 er 78.466 er 49.857 er 30.521 er 22.540 er 18.079	Volume (m ³) 0.0 0.0 0.0 0.0 0.0	(mins) 1 1 2	19 34 64 24 84 44 66 82 02 22 62 40 68 08 68 08 68 12 88
	15 m: 30 m: 60 m: 120 m: 180 m: 240 m:	.n Summ .n Summ .n Summ .n Summ .n Summ	(mm/hr) er 117.607 er 78.466 er 49.857 er 30.521 er 22.540 er 18.079	Volume (m ³) 0.0 0.0 0.0 0.0 0.0	(mins) 1 1 2	19 34 64 24 84 44 64 82 02 22 62 40 68 08 68 12 88 36
	15 m: 30 m: 60 m: 120 m: 180 m: 240 m:	.n Summ .n Summ .n Summ .n Summ .n Summ	(mm/hr) er 117.607 er 78.466 er 49.857 er 30.521 er 22.540 er 18.079	Volume (m ³) 0.0 0.0 0.0 0.0 0.0	(mins) 1 1 2	19 34 64 24 84 44 64 82 02 22 62 40 68 08 68 12 88 36 60
	15 m: 30 m: 60 m: 120 m: 180 m: 240 m:	.n Summ .n Summ .n Summ .n Summ .n Summ	(mm/hr) er 117.607 er 78.466 er 49.857 er 30.521 er 22.540 er 18.079	Volume (m ³) 0.0 0.0 0.0 0.0 0.0	(mins) 1 1 2	19 34 64 24 84 44 64 82 02 22 62 40 68 08 68 12 88 36

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ate 06/06/2			Designed	by ifle	aw atho	rstopo	- Micr
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	570 project_east		Checked				
icro Draina	ige		Source C	ontrol 2	2020.1.	3	
	-			_	_		
	Summary of Resu	<u>ilts fo</u>	<u>r 100 ye</u>	ar Retu:	rn Per:	iod (+20%)	
	Storm	Max	Max	Max	Max	Status	
	Event	Level D	oepth Infi	ltration	Volume		
		(m)	(m)	(1/s)	(m ³)		
	30 min Winter			0.2		0 K	
	60 min Winter			0.2		Flood Risk	
	120 min Winter					Flood Risk	
	180 min Winter					Flood Risk	
	240 min Winter					Flood Risk	
	360 min Winter					Flood Risk	
	480 min Winter		7.77	0 0	C7 0	Flood Risk	
	600 min Winter			0.2	67.0	Flood Risk	
	720 min Winter		/ /5	0.3	68.8	Flood Risk	
	960 min Winter		J./85	0.3	/1.4	Flood Risk Flood Risk Flood Risk Flood Risk	
	1440 min Winter		0.796	0.3	74.0	Flood Risk	
	2160 min Winter						
	2880 min Winter					Flood Risk	
	4320 min Winter 5760 min Winter					Flood Risk Flood Risk	
	7200 min Winter		770	0.3	67 7	Flood Risk	
	8640 min Winter		758	0.3	65 1	Flood Risk Flood Risk Flood Risk	
	10080 min Winter		746	0.2	62 5	Flood Risk	
		orm		Flooded			
				Volume	Time-Pea (mins)		
	Ev	ent	(mm/hr)	Volume (m³)	(mins)		
	Ev 30 m:	ent In Winter	(mm/hr) r 78.466	Volume (m³) 0.0	(mins)	34	
	Ev 30 m:	ent In Winter	(mm/hr) r 78.466	Volume (m³) 0.0	(mins)	34 64	
	Ev 30 m:	ent In Winter	(mm/hr) r 78.466	Volume (m³) 0.0	(mins)	34 64 22	
	Ev 30 m:	ent In Winter	(mm/hr) r 78.466	Volume (m³) 0.0	(mins)	34 54 22 32	
	Ev 30 m:	ent In Winter	(mm/hr) r 78.466	Volume (m³) 0.0	(mins)	34 64 22 32 40	
	Ev 30 m:	ent In Winter	(mm/hr) r 78.466	Volume (m³) 0.0	(mins)	34 64 22 32 40 58	
	Ev 30 m:	ent In Winter	(mm/hr) r 78.466	Volume (m³) 0.0	(mins)	34 64 32 32 40 58 76	
	Ev 30 m:	ent In Winter	(mm/hr) r 78.466	Volume (m³) 0.0	(mins)	34 54 22 32 40 58 76 94	
	Ev 30 m:	ent In Winter	(mm/hr) r 78.466	Volume (m³) 0.0	(mins)	34 64 22 32 40 58 76 94 08	
	Ev 30 m:	ent In Winter	(mm/hr) r 78.466	Volume (m³) 0.0	(mins)	34 54 22 32 40 58 76 94 98 82	
	Ev 30 m:	ent In Winter	(mm/hr) r 78.466	Volume (m³) 0.0	(mins)	34 54 22 32 40 58 76 94 94 93 42 96	
	Ev 30 m:	ent In Winter	(mm/hr) r 78.466	Volume (m³) 0.0	(mins)	34 54 22 32 40 58 58 76 54 20 28 29 6 36	
	Ev 30 m:	ent In Winter	(mm/hr) r 78.466	Volume (m³) 0.0	(mins)	34 64 22 82 40 58 76 94 98 88 42 96 66	
	Ev 30 m:	ent In Winter	(mm/hr) r 78.466	Volume (m³) 0.0	(mins)	34 54 52 52 58 76 94 94 95 86 86 64 44	
	Ev 30 m:	ent In Winter	(mm/hr) r 78.466	Volume (m³) 0.0	(mins)	34 54 52 52 53 58 58 54 54 56 56 54 50 50	
	Ev 30 m:	ent In Winter	(mm/hr) r 78.466	Volume (m³) 0.0	(mins)	34 54 52 32 40 58 57 69 40 96 36 56 44 44 45 0 83 60 48	

JBA Consulting		Page 3
The Library	1	raye 5
St Philips Courtyard		
Coleshill B46 3AD		
	Designed has different been	Micro
Date 06/06/2023 10:07	Designed by jflow_atherstone	Drainage
File 2023s0670 project_east		Brainacje
Micro Drainage	Source Control 2020.1.3	
	Rainfall Details	
Rainfall Model	FSR Winter Storms	Yes
Return Period (years)	100 Cv (Summer) 0.	250
Region	England and Wales Cv (Winter) 0.	250
M5-60 (mm)		15
Ratio R Summer Storms		
	Time Area Diagram	
	Total Area (ha) 0.323	
	Time (mins) Area From: To: (ha)	
	0 4 0.323	
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JBA Consulting	Page 4
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St Philips Courtyard	
Coleshill B46 3AD	Micro
Date 06/06/2023 10:07 Designed by jflow_atherstone	Drainage
File 2023s0670 project_east Checked by	brainage
Micro Drainage Source Control 2020.1.3	
Model Details	
Storage is Online Cover Level (m) 0.900	
Swale Structure	
Infiltration Coefficient Base (m/hr) 0.00750 Length (m) Infiltration Coefficient Side (m/hr) 0.00750 Side Slope (1:X) Safety Factor 2.0 Slope (1:X) Porosity 1.00 Cap Volume Depth (m) Invert Level (m) 0.000 Cap Infiltration Depth (m) Base Width (m) 1.0	3.0 90.0 0.000
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Swale East 2

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e 06/06/2023	10:10		Desi	gned	by jflo	ow athe	erstone
e 2023s0670 p	roject eas	t				_	
ro Drainage	_				ontrol 2	2020.1	.3
Summ	ary of Resu	ults f	or 10	0 ye	ar Retu	rn Per	iod (+20%)
					345 minut		
	Storm	Max	Max		Max	Max	Status
	Event	Level	Depth	Infi	ltration	Volume	
	5 min Summer 30 min Summer	(m)	(m)		(1/s)	(m³)	
1	5 min Summer	0.817	0.817		0.1	23.0	ОК
	30 min Summer	0.911	0.911		0.1	30.6	ОК
e	50 min Summer	0.996	0.996		0.1	38.8	ОК
12	20 min Summer	1.072	1.072		0.1	47.2	Flood Risk
18	30 min Summer	1.112	1.112		0.1	52.0	Flood Risk
24	10 min Summer	1.138	1.138		0.1	55.3	Flood Risk
36	30 min Summer	1.174	1.174		0.2	60.3	Flood Risk
48	30 min Summer	1.199	1.199		0.2	63.8	Flood Risk
60	0 min Summer	1.217	1.217		0.2	66.4	Flood Risk
72	0 min Summer	1.232	1.232		0.2	68.5	Flood Risk
96	0 min Summer	1.252	1.252		0.2	71.7	Flood Risk
144	10 min Summer	1.2/6	1.2/6		0.2	75.4	Flood Risk
210	0 min Summer	1 204	1 291		0.2	78.4	Flood Risk
200	0 min Summer	1 202	1 202		0.2	79.1	Flood Risk
432	50 min Summer	1 289	1 289		0.2	77 5	Flood Risk
720)0 min Summer	1.283	1.283		0.2	76.6	Flood Risk
864	10 min Summer	1.277	1.277		0.2	75.6	Flood Risk
1008	30 min Summer	1.270	1.270		0.2	74.4	Flood Risk
1	5 min Winter	0.817	0.817		0.1	23.0	ОК
	St	orm	R	ain	Flooded	Time-Pe	ak
		orm			Flooded Volume	Time-Pe (mins)	
	Ev	ent	(mn	/hr)	Volume	(mins)	
	Ev	ent	(mn	/hr)	Volume	(mins)	
	Ev	ent	(mn	/hr)	Volume	(mins)	
	Ev	ent	(mn	/hr)	Volume	(mins)	
	Ev	ent	(mn	/hr)	Volume	(mins)	
	Ev	ent	(mn	/hr)	Volume	(mins)	
	Ev	ent	(mn	/hr)	Volume	(mins)	
	Ev	ent	(mn	/hr)	Volume	(mins)	
	Ev	ent	(mn	/hr)	Volume	(mins)	
	Ev	ent	(mn	/hr)	Volume	(mins)	
	Ev	ent	(mn	/hr)	Volume	(mins)	
	Ev	ent	(mn	/hr)	Volume	(mins)	
	Ev	ent	(mn	/hr)	Volume	(mins)	
	Ev	ent	(mn	/hr)	Volume	(mins)	
	Ev	ent	(mn	/hr)	Volume	(mins)	
	Ev	ent	(mn	/hr)	Volume	(mins)	
	Ev	ent	(mn	/hr)	Volume	(mins)	
	Ev	ent	(mn	/hr)	Volume	(mins)	
	Ev	ent	(mn	/hr)	Volume	(mins)	
	Ev	ent	(mn	/hr)	Volume	(mins)	

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St Philips							
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ate 06/06/		г	Designed	bu ifl	or oth	aratono	Micro
			-		ow_athe	erstone	Draina
	670 project_eas						
licro Drain	age	5	Source C	ontrol 3	2020.1	.3	
	Cummanu of Doo	ulto fo	- 100	an Datu	nn Don	ind (120%)	
	Summary of Res	ults io	r 100 ye	<u>ar ketu</u>	<u>rn Per</u>	<u>100 (+208)</u>	
	Storm	Max	Max	Max	Max	Status	
	Event	Level D	epth Infi	ltration	Volume		
		(m)	(m)	(1/s)	(m³)		
	20	0 011 0	011	0 1	20 0	0.11	
	30 min Winter 60 min Winter			0.1	30.6 38.8	ОК	
	120 min Winter					Flood Risk	
	180 min Winter					Flood Risk	
	240 min Winter					Flood Risk	
	360 min Winter					Flood Risk	
	480 min Winter					Flood Risk	
	600 min Winter			0.2	66.5	Flood Risk	
	720 min Winter			0.2	68.6	Flood Risk	
	960 min Winter			0.2	71.8	Flood Risk	
	1440 min Winter	: 1.277 1	.277	0.2	75.6	Flood Risk	
	2160 min Winter					Flood Risk	
	2880 min Winter					Flood Risk	
	4320 min Winter			0.2	78.2	Flood Risk Flood Risk	
	5760 min Winter			0.2	77.3	Flood Risk	
	7200 min Winter			0.2	75.9	Flood Risk Flood Risk Flood Risk	
	8640 min Winter 10080 min Winter			0.2	74.3	Flood Risk	
		torm		Flooded			
		torm vent		Volume	Time-Pe (mins)		
	E	vent		Volume (m³)	(mins)		
	E 30 m 60 m	vent in Winter in Winter	(mm/hr) r 78.466 r 49.857	Volume (m ³) 0.0 0.0	(mins)		
	E 30 n 60 n 120 n	vent in Winter in Winter in Winter	(mm/hr) r 78.466 r 49.857 r 30.521	Volume (m ³) 0.0 0.0 0.0	(mins)	34 64 22	
	30 m 60 m 120 m 180 m	vent in Winter in Winter in Winter in Winter	(mm/hr) r 78.466 r 49.857 r 30.521 r 22.540	Volume (m ³) 0.0 0.0 0.0 0.0	(mins) 1 1	34 64 22 82	
	30 m 60 m 120 m 180 m 240 m	vent in Winter in Winter in Winter in Winter	(mm/hr) r 78.466 r 49.857 r 30.521 r 22.540 r 18.079	Volume (m ³) 0.0 0.0 0.0 0.0 0.0	(mins) 1 1 2	34 64 22 82 42	
	30 m 60 m 120 m 180 m 240 m	vent in Winter in Winter in Winter in Winter	(mm/hr) r 78.466 r 49.857 r 30.521 r 22.540 r 18.079	Volume (m ³) 0.0 0.0 0.0 0.0 0.0	(mins) 1 1 2	34 64 22 82 42 60	
	30 n 60 n 120 n 180 n 240 n 360 n 480 n	vent in Winter in Winter in Winter in Winter in Winter in Winter	(mm/hr) r 78.466 r 49.857 r 30.521 r 22.540 r 18.079 r 13.261 r 10.625	Volume (m ³) 0.0 0.0 0.0 0.0 0.0 0.0 0.0	(mins) 1 1 2 3 4	34 64 22 82 42 60 78	
	30 n 60 n 120 n 180 n 240 n 360 n 480 n	vent in Winter in Winter in Winter in Winter in Winter in Winter	(mm/hr) r 78.466 r 49.857 r 30.521 r 22.540 r 18.079 r 13.261 r 10.625	Volume (m ³) 0.0 0.0 0.0 0.0 0.0 0.0 0.0	(mins) 1 1 2 3 4	34 64 22 82 42 60 78 96	
	30 n 60 n 120 n 180 n 240 n 360 n 480 n	vent in Winter in Winter in Winter in Winter in Winter in Winter	(mm/hr) r 78.466 r 49.857 r 30.521 r 22.540 r 18.079 r 13.261 r 10.625	Volume (m ³) 0.0 0.0 0.0 0.0 0.0 0.0 0.0	(mins) 1 1 2 3 4	34 64 22 82 42 60 78 96 14	
	30 n 60 n 120 n 180 n 240 n 360 n 480 n	vent in Winter in Winter in Winter in Winter in Winter in Winter	(mm/hr) r 78.466 r 49.857 r 30.521 r 22.540 r 18.079 r 13.261 r 10.625	Volume (m ³) 0.0 0.0 0.0 0.0 0.0 0.0 0.0	(mins) 1 1 2 3 4	34 64 22 82 42 60 78 96 14 46	
	30 n 60 n 120 n 180 n 240 n 360 n 480 n	vent in Winter in Winter in Winter in Winter in Winter in Winter	(mm/hr) r 78.466 r 49.857 r 30.521 r 22.540 r 18.079 r 13.261 r 10.625	Volume (m ³) 0.0 0.0 0.0 0.0 0.0 0.0 0.0	(mins) 1 1 2 3 4	34 64 22 82 42 60 78 96 14 46 12	
	30 n 60 n 120 n 180 n 240 n 360 n 480 n	vent in Winter in Winter in Winter in Winter in Winter in Winter	(mm/hr) r 78.466 r 49.857 r 30.521 r 22.540 r 18.079 r 13.261 r 10.625	Volume (m ³) 0.0 0.0 0.0 0.0 0.0 0.0 0.0	(mins) 1 1 2 3 4	34 64 22 82 42 60 78 96 14 46 12 96	
	30 n 60 n 120 n 180 n 240 n 360 n 480 n	vent in Winter in Winter in Winter in Winter in Winter in Winter	(mm/hr) r 78.466 r 49.857 r 30.521 r 22.540 r 18.079 r 13.261 r 10.625	Volume (m ³) 0.0 0.0 0.0 0.0 0.0 0.0 0.0	(mins) 1 1 2 3 4	34 64 22 82 42 60 78 96 14 46 12 96 40	
	30 n 60 n 120 n 180 n 240 n 360 n 480 n	vent in Winter in Winter in Winter in Winter in Winter in Winter	(mm/hr) r 78.466 r 49.857 r 30.521 r 22.540 r 18.079 r 13.261 r 10.625	Volume (m ³) 0.0 0.0 0.0 0.0 0.0 0.0 0.0	(mins) 1 1 2 3 4	34 64 22 82 42 60 78 96 14 46 12 96 40 48	
	30 n 60 n 120 n 180 n 240 n 360 n 480 n	vent in Winter in Winter in Winter in Winter in Winter in Winter	(mm/hr) r 78.466 r 49.857 r 30.521 r 22.540 r 18.079 r 13.261 r 10.625	Volume (m ³) 0.0 0.0 0.0 0.0 0.0 0.0 0.0	(mins) 1 1 2 3 4	34 64 22 82 42 60 78 96 14 46 12 96 40 40 48 32	
	30 n 60 n 120 n 180 n 240 n 360 n 480 n	vent in Winter in Winter in Winter in Winter in Winter in Winter	(mm/hr) r 78.466 r 49.857 r 30.521 r 22.540 r 18.079	Volume (m ³) 0.0 0.0 0.0 0.0 0.0 0.0 0.0	(mins) 1 1 2 3 4	34 64 22 82 42 60 78 96 14 46 12 96 40 48 32 36	

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St Philips Courtyard			
Coleshill B46 3AD			Micro
Date 06/06/2023 10:10		Designed by jflow_atherstone	
File 2023s0670 project_east		Checked by	Diamaye
Micro Drainage		Source Control 2020.1.3	1
	<u>Ra</u>	infall Details	
Rainfall Model		FSR Winter Storms	(es
Return Period (years) Region	Engla	and and Wales Cv (Winter) 0.2	250
M5-60 (mm)	2	20.500 Shortest Storm (mins)	15
Ratio R		0.363 Longest Storm (mins) 100	
Summer Storms		Yes Climate Change %	+20
	<u>Tir</u>	ne Area Diagram	
	Tot	al Area (ha) 0.313	
		ime (mins) Area om: To: (ha)	
		0 4 0.313	
		0 4 0.515	
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St Philips Courtyard		
Coleshill B46 3AD		Micro
Date 06/06/2023 10:10	Designed by jflow_atherstone	
File 2023s0670 project_east	Checked by	Drainage
Micro Drainage	Source Control 2020.1.3	
N	Model Details	
_		
Storage is Or	nline Cover Level (m) 1.300	
<u></u>	vale Structure	
Infiltration Coefficient Base (m	n/hr) 0.00750 Length (m	98.0
Infiltration Coefficient Side (m		
Safety Fa	actor 2.0 Slope (1:X) 26.1
Porc	osity 1.00 Cap Volume Depth (m) 0.000
Invert Level	. (m) 0.000 Cap Infiltration Depth (m n (m) 1.0) 0.000
Base Width	1 (m) 1.U	
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le 2023s0670 pi	:oject_wes	t					
cro Drainage			Sour	ce C	ontrol :	2020.1	.3
Summa	ary of Res	ults f	<u>or 10</u>	0 ye	ar Retu	rn Per	iod (+20%
	Н	alf Dra	in Time	e : 4	126 minut	tes.	
	Storm	Max	Max		Max	Max	Status
	Event	Level	Depth	Infi	ltration	Volume	
		(m)	(m)		(l/s)	(m³)	
							V.57 6.149
1.	5 min Summer	0.746	0.746		0.4	104.0	ОК
30) min Summer	0.833	0.833		0.5	138.5	O K
60) min Summer	. 0.911	0.911		0.6	1/5.5	riood Risk
120) min Summer	1 017	1 017		0.6	213.7	Flood Risk
180) min Summer	. 1.01/	1.011		0.7	235.4	Flood Risk
240) min Summer	1 074	1.074		0.7	230.4	Flood Risk
36) min Summer	. 1.0074	1 007		0.7	202.0	Flood Bick
480) min Summou	- 1 114	1 114		0.0	200.3	Flood Rick
000 701) min Summon	- 1 12A	1 126		0.8	300.2	Flood Rick
961) min Summer	- 1.145	1.145		0.0	323 1	Flood Riek
144) min Summer	1.166	1.166		0.9	339.6	Flood Risk
216) min Summeı	1.178	1.178		0.9	349.5	Flood Risk
288) min Summeı	1.180	1.180		0.9	351.0	Flood Risk
4320) min Summer	1.179	1.179		0.9	349.8	Flood Risk
576) min Summer	1.175	1.175		0.9	346.5	Flood Risk
720) min Summer	1.169	1.169		0.9	342.1	Flood Risk
864) min Summer	1.162	1.162		0.9	337.0	Flood Risk
10080) min Summer	1.155	1.155		0.8	331.2	Flood Risk
1!	5 min Summer 7 min Summer 9 min Summer	0.746	0.746		0.4	104.0	O K
	St	torm	Ra	ain	Flooded	Time-Pe	ak
	E	vent	(mm	/hr)	Volume	(mins)	1
					(m³)		
	15 m	in Summ	er 117	607	0 0		19
	30 m	in Summ	or 70	466	0.0		34
	60 m	in Summ	er 49	.857	0.0		64
	120 m	in Summ	er 30	.521	0.0	1	24
	180 m	in Summ	er 22	.540	0.0	1	84
	240 m	in Summ	er 18	.079	0.0	2	44
	360 m	in Summ	er 13	.261	0.0	3	64
	480 m	in Summ	er 10	.625	0.0	4	84
	600 m	in Summ	er 8	.940	0.0	6	02
	720 m	in Summ	er 7	.759	0.0	7	22
	960 m	in Summ	er 6	.200	0.0	9	62
	1440 m	in Summ	er 4	.511	0.0	14	42
	2160 m	in Summ	er 3	.275	0.0	21	60
	2880 m	in Summ	er 2	.606	0.0	27	40
	2000 1	in Summ	er 1	.886	0.0	34	16
	4320 m	In Summ		407	0 0	41	52
	4320 m 5760 m	in Summ	er 1	.491	0.0		
	4320 m 5760 m 7200 m	in Summ in Summ	er 1 er 1	.252	0.0	49	68
	4320 m 5760 m 7200 m 8640 m	in Summ in Summ in Summ	er 1 er 1 er 1	.252	0.0	49 57	68 92
	4320 m 5760 m 7200 m 8640 m 10080 m	in Summ in Summ in Summ in Summ	er 1 er 1 er 1 er 0	.252 .082 .957	0.0 0.0 0.0	49 57 66	68 92 48
	15 m 30 m 60 m 120 m 180 m 360 m 480 m 720 m 960 m 1440 m 2880 m 4320 m 5760 m 7200 m 640 m 10080 m 10080 m	in Summ in Summ in Summ in Summ in Summ	er 1 er 1 er 1 er 0 er 117	.252 .082 .957 .607	0.0 0.0 0.0 0.0	49 57 66	68 92 48 19

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The Library							
St Philips Court	yard						The second
Coleshill B46 3	AD						Micro
Date 06/06/2023 10:14		E	esigned	by jflo	ow athe	erstone	
File 2023s0670 project_west			Checked	by	_		DIgilig
Micro Drainage			Source C	ontrol 2	2020.1	.3	
Summ	ary of Resu	lts for	<u>r 100 ye</u>	ar Retu	rn Per	iod (+20%)	
	Storm	Max 1	Max	Max	Max	Status	
	Event		epth Infi				
		(m)	(m)	(1/s)	(m ³)		
3	30 min Winter	0.833 0	.833	0.5	138.5	ОК	
	50 min Winter					Flood Risk	
	20 min Winter					Flood Risk	
	30 min Winter			0.7	235.5	Flood Risk	
	10 min Winter					Flood Risk	
	50 min Winter			0.7		Flood Risk	
	30 min Winter)0 min Winter					Flood Risk Flood Risk	
	20 min Winter					Flood Risk	
	50 min Winter					Flood Risk	
144	10 min Winter	1.167 1	.167	0.9	340.5	Flood Risk	
	50 min Winter					Flood Risk	
	30 min Winter					Flood Risk	
	20 min Winter			0.9	349.8	Flood Risk	
	50 min Winter)0 min Winter			0.9	345.0	Flood Risk Flood Risk Flood Risk	
	10 min Winter			0.8	330.2	Flood Risk	
	30 min Winter			0.8	321.8	Flood Risk	
	Sto			Flooded	Time-Pe	ak	
	Eve	nt	(mm/hr)	Volume (m³)	(mins)		
	20 min	Winter	70 466	0.0		34	
			78.466			54 64	
	120 mir	n Winter	49.857 30.521	0.0		22	
			22.540			82	
			18.079		2	42	
	360 mir	n Winter	13.261	0.0	3		
	480 mir	n Winter	10.625 8.940	0.0	4		
	600 mir	n Winter	8.940 7.759 6.200 4.511 3.275	0.0	5	96 14	
	720 M11 960 mir	n Winter N Winter	6.200	0.0	9		
	1440 mir	n Winter	4.511	0.0	14		
	2160 mir	n Winter	3.275	0.0	20		
	2880 mir	n Winter	2.606	0.0	27	36	
			1.886		34		
			1.497				
			1.252				
	10080 mir	. Winter	1.082 0.957	0.0	62 71		
	72000 1011			0.0	, 1		

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St Philips Courtyard		
Coleshill B46 3AD		Micro
Date 06/06/2023 10:14	Designed by jflow_atherstone	Drainage
File 2023s0670 project_west		brainage
Micro Drainage	Source Control 2020.1.3	
	Rainfall Details	
Rainfall Model Return Period (years)	FSR Winter Storms 1 100 Cv (Summer) 0.2	
	England and Wales Cv (Winter) 0.2	
M5-60 (mm)	20.500 Shortest Storm (mins)	
Ratio R		
Summer Storms	Yes Climate Change % -	+20
	<u>Time Area Diagram</u>	
	Total Area (ha) 1.418	
	Time (mins) Area From: To: (ha)	
	0 4 1.418	
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Coleshill B46 3AD		
Date 06/06/2023 10:14	Designed by ifley atheneters	MICLO
	Designed by jflow_atherstone	Drainage
File 2023s0670 project_west		
Micro Drainage	Source Control 2020.1.3	
<u>1</u>	Model Details	
Storage is O	nline Cover Level (m) 1.200	
<u></u>	vale Structure	
Infiltration Coefficient Base (m		
Infiltration Coefficient Side (m		
Safety Fa	actor 2.0 Slope (1:X osity 1.00 Cap Volume Depth (m) 150.0
	(m) 0.000 Cap Infiltration Depth (m	
Base Width		
	2. 2020 Terran	
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Swale West 2

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e 06/06/2023 :			Desi	ned	by ifle	ow athe	erstone
e 2023s0670 p:		+					51000000
	Loject_wes				-	2020 1	2
ro Drainage			Sour	ce uc	ntrol 2	2020.1	
Summa	ary of Resi	ilts f	or 10	0 vez	r Retu	rn Per	iod (+20
<u>o unine</u>	iry or nest	<u>AT CO T</u>	01 10	<u>v ye</u> c	II NECU	LII LOL	104 (120
	Ha	lf Dra	in Tim	e : 37	89 minut	es.	
	Storm	Max	Max		Max	Max	Status
	Event	Level	Depth	Infil	tration	Volume	
		(m)	(m)	(1/s)	(m³)	
1		0 (02	0 (02		0.1	20.2	0
5 T	5 min Summer 0 min Summer 0 min Summer	0.093	0.093		0 1	30 0	0
5	0 min Summer	0.847	0.847		0.2	49.4	Flood Ris
	0 min Summer 0 min Summer				0.2	60.1	Flood Ris
	0 min Summer				0.2	66.1	Flood Ris
					0.2	70.3	Flood Ris
36	0 min Summer	0.999	0.999		0.2	76.5	Flood Ris
48	0 min Summer	1.020	1.020		0.2	80.8	Flood Ris
60	0 min Summer 0 min Summer 0 min Summer 0 min Summer 0 min Summer	1.035	1.035		0.2	84.1	Flood Ris Flood Ris Flood Ris Flood Ris Flood Ris Flood Ris
72	0 min Summer	1.047	1.047		0.2	86.7	Flood Ris
96	0 min Summer	1.064	1.064				Flood Ris
	0 min Summer						Flood Ris
216	0 min Summer	1.092	1.092		0.3	96.9	Flood Ris
288) min Summer) min Summor	1.092	1.092		0.3	97.1	Flood Ris Flood Ris Flood Ris Flood Ris Flood Ris Flood Ris
432	0 min Summer	1.086	1.086		0.3	95.5	Flood Ris
720	0 min Summer	1.079	1.079		0.3	94.1	Flood Ris
864	0 min Summer	1.072	1.072		0.3	92.4	Flood Ris
1008	0 min Summer	1.065	1.065		0.3	90.6	Flood Ris
1	5 min Winter	0.693	0.693		0.1	29.3	0
	0 min Summer 0 min Summer 0 min Summer 0 min Summer 0 min Summer 0 min Summer 5 min Winter						
		orm	1	12	Flooded Volume	1-1	
	Ev	enc	(1101	<i>(((((((((((((</i>	(m ³)	(mrus)	
	15			607			1.0
	30 m	in Summ	er II/	.007	0.0		31
	50 III. 60 m	in Summ	er 10	. 857	0.0		64
	120 m	in Summ	er 30	.521	0.0	1	24
	180 m	in Summ	er 22	.540	0.0	1	84
	240 m	in Summ	er 18	.079	0.0	2	44
	360 m.	in Summ	er 13	.261	0.0	3	64
	480 m	in Summ	er 10	.625	0.0	4	84
	600 m	in Summ	er 8	.940	0.0	6	02
	720 m	in Summ	er 7	.759	0.0	7	22
	960 m:	in Summ	er 6	.200	0.0	9	62
	1440 m	in Summ	er 4	.511	0.0	14	42
	2160 m	in Summ	er 3	.215	0.0	21	24
	∠880 m. 4320 m.	in Summ	er 2 or 1	.000	0.0	20	24 28
	5760 m	in Summ	er 1	. 497	0.0	40	88
	7200 m	in Summ	er 1	.252	0.0	49	04
						57	10
	8640 m	in Summ	er 1	.082	0.0	57	12
	8640 m: 10080 m:	in Summ in Summ	er 1 er 0	.082 .957	0.0	65	52
	15 m. 30 m. 60 m. 120 m. 120 m. 240 m. 240 m. 360 m. 480 m. 960 m. 2160 m. 2160 m. 2260 m. 35760 m. 7200 m. 8640 m. 10080 m. 15 m.	in Summ in Summ in Wint	er 1 er 0 er 117	.082 .957 .607	0.0 0.0 0.0	65	52 19

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ate 06/06/2023 10:17		Designed	hy if	ow ath	arstone	MI
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le 2023s0670 project_	west	Checked				
lcro Drainage		Source (Control 2	2020.1	.3	
Summary of	Results fo	or 100 ye	ear Retu	rn Per	iod (+20%)	
Storm	Max	Max	Max	Max	Status	
Event	Level	Depth Inf	iltration	Volume		
	(m)	(m)	(l/s)	(m³)		
20	0 774	0 774	0 1	20.0	0.77	
	nter 0.774 nter 0.847		0.1			
	nter 0.847		0.2		Flood Risk Flood Risk	
	nter 0.912		0.2		Flood Risk	
	nter 0.946		0.2		Flood Risk	
	nter 0.968				Flood Risk Flood Risk	
	nter 1.020 nter 1.036				Flood Risk Flood Risk	
	nter 1.036				Flood Risk Flood Risk	
960 min Wi	nter 1.064 nter 1.083 nter 1.094 nter 1.096 nter 1.090	1.064			Flood Risk	
1440 min Wi	nter 1.083	1.083	0.3	94.9	Flood Risk	
2160 min Wi	nter 1.094	1.094	0.3	97.5	Flood Risk	
2880 min Wi	nter 1.096	1.096	0.3	97.9	Flood Risk	
4320 min Wi	nter 1.090	1.090	0.3	96.5	Flood Risk	
5760 min Wi	nter 1.083	1.083	0.3	94.9	Flood Risk	
2100 min Wi 2880 min Wi 4320 min Wi 5760 min Wi 7200 min Wi 8640 min Wi 10080 min Wi	nter 1.073	1.073	0.3	92.6	Flood Risk	
8640 min Wi	nter 1.063	1.063	0.3	90.2	Flood Risk	
	Storm Event		Flooded Volume	Time-Pe (mins)		
			(m ³)			
	30 min Winte	er 78.466	0.0		34	
	60 min Winte				64	
1	20 min Winte	er 30.521	0.0	1	22	
1	80 min Winte	er 22.540	0.0	1	82	
2	40 min Winte	er 18.079	0.0	2	42	
3	60 min Winte	er 13.261	0.0	3	60	
4	80 min Winte	er 10.625	0.0	4	78	
6	00 min Winte	er 8.940	0.0	5	96	
7	20 min Winte	er 7.759	0.0	7	14	
9	60 min Winte	er 6.200	0.0	9	44	
14	40 min Winte	er 4.511	0.0	14		
21	60 min Winte	er 3.275	0.0	20		
21	80 min Winte	er 2.606	0.0	27		
43	20 min Winte	er 1.886	0.0	34		
57	60 min Winte	-r 1 497	0.0	43		
57 72	00 min Winte	1.197	0.0	52		
2 / 2	40 min Winte	ar 1 097	0.0	61		
100	80 min Winte	ar 0.057	0.0	70		
	80 min Winte 40 min Winte 60 min Winte 80 min Winte 20 min Winte 40 min Winte 60 min Winte 80 min Winte 60 min Winte 60 min Winte 40 min Winte 80 min Winte 80 min Winte					

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Coleshill B46 3AD		Micro
Date 06/06/2023 10:17	Designed by jflow_atherstone	Drainage
File 2023s0670 project_west	Checked by	Diamage
Micro Drainage	Source Control 2020.1.3	
	<u>Rainfall Details</u>	
Rainfall Model Return Period (years)	FSR Winter Storms 100 Cv (Summer) 0.	
Region	England and Wales Cv (Winter) 0.	250
M5-60 (mm)	20.500 Shortest Storm (mins)	15
Ratio R		
Summer Storms	Yes Climate Change %	+20
	<u>Time Area Diagram</u>	
	Total Area (ha) 0.399	
	Time (mine) Bree	
	Time (mins) Area From: To: (ha)	
	0 4 0.399	
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Coleshill B46 3AD		Micro
Date 06/06/2023 10:17	Designed by jflow_atherstone	Drainage
File 2023s0670 project_west		Diamage
Micro Drainage	Source Control 2020.1.3	
Model Details		
Storage is Online Cover Level (m) 1.100		
Swale Structure		
Infiltration Coefficient Base (m Infiltration Coefficient Side (m		
Safety Fa	actor 2.0 Slope (1:X) 51.1
Porc	sity 1.00 Cap Volume Depth (m) 0.000
	. (m) 0.000 Cap Infiltration Depth (m n (m) 1.0	0.000
base widtr	1 (m) 1.0	
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